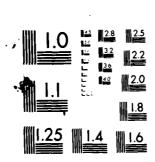
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MX SITING INVESTIGATION GEOTECHNICAL EVALUATION

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VERIFICATION STUDY PAHROC VALLEY, NEVADA VOLUME II - GEOTECHNICAL DATA

PREPARED FOR BALLISTIC MISSILE OFFICE (BMO) NORTON AIR FORCE BASE, CALIFORNIA



MX SITING INVESTIGATION GEOTECHNICAL EVALUATION

VERIFICATION STUDY - PAHROC VALLEY NEVADA

VOLUME II - GEOTECHNICAL DATA

Prepared for:

U.S. Department of the Air Force Ballistic Missile Office (BMO) Norton Air Force Base, California 92409

Prepared by:

Ertec Western, Inc. 3777 Long Beach Boulevard Long Beach, California 90807

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FOREWORD

This volume of geotechnical data was compiled for the Department of the Air Force, Ballistic Missile Office (BMO), in compliance with Contract No. F04704-80-C-0006, CDRL Item 004A6. It contains the field data and laboratory test results from the Verification investigation of Pahroc Valley. A synthesis of these data are available in Volume I (E-TR-27-PA-I).

The data in each section of this volume are preceded by an explanation of the format and terms used in the compilation.

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1.0 ACTIVITY MAP AND GEOLOGRAPHIC COORDINATES

Explanation: Locations of all field activities are shown in Drawing II-1-1, Activity Location Map (in pocket). The geodetic and Universal Transverse Mercator (UTM) coordinates of all activities are listed in Table II-1-1.

ACT	G	EDDETIC	c co	ORD.	UTM CO ZONE N(KM)	ORD.
ID.	¹	_AT.	L	ONG.	ZONE	. 12
	DEG 		DEG	MIN	N(KM)	E(KM)
BBB TNO	- + -					
BORING						
PA- B01	37	38. 59	115	4. 90	4167. 76	669. 24
PA- B02	37	36. 59	115	3. 90	4164.08	670. 79
PA- B03	37	35. 50	115	5. 58	4162. 02	668. 37
CPT SIT	ES					
PA- CO1	- -	38, 29	115	0 13	4167. 34	676 2B
PA- CO2	37	38. 05	115	1.20	4166.87	674.71
PA- CO3					4165.83	
PA- C04						
PA- C05					4164.08	
PA- CO6					4167.76	
PA- C07	37	38. 77	115	6.00	4168.04	667. 62
PA- COB	37	38. 96	115	7. 05	4168. 37	666.08
PA- C09	37	39. 05	115	8.01	4168. 51 4163. 89	664. 66
PA- C10	37	36. 51	115	5. 03	4143. 89	669. 14
PA- C11	37	36. 01	115	8. 39	4162. 87	664. 21
PA- C12	37	35. 87	115	7. 45	4162. 64 4162. 35	665. 60
PA- C14	37	35. 50	115	5. 58	4162. 02	668. 37
PA- C15					4161.65	
					4161. 17	
PA- C17	37	32. 69	115	9. 19	4156. 71 4155. 32	663. 15
PA- C18	37	31. 92	115	8. 36	4155. 32	664. 40
PA- 019	3/	31. 22	115	7. 53	4154.04	665.65
PA- C20	3/	30. 42	115	6. 71	4152. 59 4151. 46	667. 19
PA- 022	3/	36. 82	114	76. 74	4164. 72	681.32
PA- C23					4163.03	
PA- 024	3/	33.11	114	77. Y7	4161.59	682. 76
PA- 023	3/	34. //	114	76. 73 57. 77	4160. 95 4159. 77	681. /1
PA- C20	3/	34. 13	114	3/. 3/ ED 04	4159.77	470 50
					4158.76	
GEOLOGI						
			_			
					4164. 90	
PA-GS02	37	36. 73	114	55. 28	4164.61	683. 47



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GEODETIC AND UTM COORDINATES
OF ACTIVITY LOCATIONS
PAHROC VALLEY, NEVADA
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TABLE II-1-1

ACT		EDDETIC			UTM CO	
ID.		_AT. MIN	DEG	DNG. MIN	ZONE N(KM)	12 E(KM)
	DEG	11111	DEG	11114	NONE	EVANO
FA-G503	37	37. 05	115	1. 55	4165.01	674. 24
PA~GSO4	37	35. 48	115	5. 46	4161.99	668. 54
PA-GS05	37	36.00	115	8. 48	4162.86	664. 07
PA-G506	37	32. 46	115	9.06	4156, 29	663. 36
PA~GS07	37	34. 39	115	4.41	4159. 99	670.13
PA~GS08	37	39. 54	115	4. 74	4169. 52	669. 45
PA-GS09	37	39.00	115	7. 69	4168.42	665. 14
PA-GS10	37	36, 60	115	1. 68	4164. 16	674. 07
PA~GS11	37	34. 95	115	3. 12	4161.07	672. 01
PA-G512	37	34. 76	115	4. 09	4160.68	670. 59
PA-GS13	37	32. 64	115	6. 29	4156.71	667. 43
PA-GS14	37	31 37	115	6. 07	4154.37	667. 80
PA-G515	37	29. 59	115	5. 28	4151.10	669. 03
PA-GS16	37	30. 96	115	7. 27	4153.57	666. 05
PA-G517	37	31.20	115	9. 16	4153. 96	663. 25
PA-GS18	37	32. 68 32. 55	115	9. 51 10. 02	4156. 69 4156. 44	662. 68
PA-G519 PA-G520	37	33. 25	115 115	9, 25	4156. 44	661. 9 3 663. 05
PA-G520	37 37	34. 91	115	7. 23 7. 81	4160.86	665. 11
PA-GS22	37	36. 02	115	8.64	4162.89	663. 84
PA-GS23	37	36. 30	115	7. 18	4163. 44	665. 9 9
PA-G524	37	36. 49	115	6.48	4163.82	667.00
PA-GS25	37	36. 76	115	2. 61	4164. 43	672. 68
PA-GS26	37	37. 93	115	1.08	4166.64	674.89
PA-GS27	37	38. 88	115	1. 18	4168.39	674. 70
PA-GS28	37	38. 19	115	3. 25	4167.06	671.69
PA-GS29	37	36, 70	115	3. 41	4164.30	671.52
PA-GS30	37	39. 69	115	8, 56	4169.67	663. 82
PA-GS31	37	36. 03	115	7. 74	4162. 93	665. 16
PA-GS32	37	34. 03	115	8.06	4159. 22	664. 76
PA-GS33	37	37. 55	115	8. 89	4165.71	663. 41
PA-GS34	37	35. 83	114	59. 59	4162. 82	677. 17
PA-GS35	37	34.64	114	58. 45	4160.65	678. 89
PA-GS36	37	33. 72	114	57. 81	4158. 97	679. 87
PA-G537	37	31.62	114	58. 75	4155.06	678. 58
PA-GS38	37	20. 10	114	59. 87	4152. 20	676. 98
PA-G539	37	35.00	114	56. 15	4161.38	682. 26
PA-G540	37	36. 03	114	57. 80	4163. 24	679. 79
PA-GS41	37	31. 33	114	56. 08	4154.60	682. 52
PA-GS42	37	30. 45	114	57. 68	4152. 93	680. 19



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GEODETIC AND UTM COORDINATES
OF ACTIVITY LOCATIONS
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TABLE II-1-1

ACT	GECDETIC	COORD. LONG. DEG MIN	UTM CO	ORD.
ID.	LAT.	LONG.	ZONE	12
D	EG MIN	DEG MIN	N(KM)	E(KM)
	~~~~~			
n	<b>~</b> ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	444 50 04	445/ 07	
PA-G543	37 32.29	114 59. 21	4106.27	677. 87
PA-G544	37 33.21	114 57.47 114 55.14	4158.02	680. 39 683. 72
PA-0545	37 35.81	114 54.61	4102.74	604. 47 477 10
PA-G54/	37 33 49	114 59.57 115 0.33	4103.JZ	677.10
PA-0940	27 22 40	114 55.78	4157 19	492 91
ידעטיייי	3/ 32.07	114 33.76	719/. 12	GOZ. 71
REFRACTI	ON LINES			
DA- CO1	27 20 20	115 0.13	4147 74	474 20
		115 5.58		
PA- 502	37 35 00	115 2 93	4162.02	672. 29
PA- 504	37 32 69	115 2. 93 115 9. 19	4156 71	663 15
PA- S05	37 29 80	115 5.80	4151.46	668. 26
PA- 506	37 32 90	114 58.65	4157.41	678. 66
PA- 507	37 35.11	114 58. 65 114 55. 95	4161. 59	682. 56
KESISIIV	ITY LINES	Š		
PA- PO1	27 20 20	115 0.13	4147 74	474 20
PA~ ROZ	37 35 00	115 5.58 115 2.93	4162.02	672 29
PA- RO4	37 32 69	115 9.19	4154 71	663 15
PA- 805	37 29 80	115 5 80	4151 4A	448 24 448
PA- 806	37 32 90	114 58.65	4157 41	678.66
PA- ROZ	37 35.11	114 55. 95	4161.59	682.56
	<b>.</b>			
SURFICIA	L SOIL SA	AMPLES		
PA-CS03	37 37.51	115 2.28	4165. 83	673. 15
		115 7.05		666. 08
PA-CS12	37 35.87	115 7.45	4162.64	
PA-CS13	37 35.69	115 7.45 115 6.38	4162. 64 4162. 35	
PA-CS15	37 35.26	115 4.37	4161.61	670.15
PA-CS17	37 32.69	115 9.19 115 7.53	4156.71	663. 15
PA-CS19	37 31.22	115 7.53	4154.04	665. 65
PA-CS23	<b>37 35</b> . 90	114 56.48	4163. 03	681.75
PA-CS25	37 34.77	114 56. 48 114 56. 53 114 58. 01	4160. 95	681.71
PA-CS27	37 33.61	114 58.01	4158.01	679. 58



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GEODETIC AND UTM COORDINATES
OF ACTIVITY LOCATIONS
PAHROC VALLEY, NEVADA
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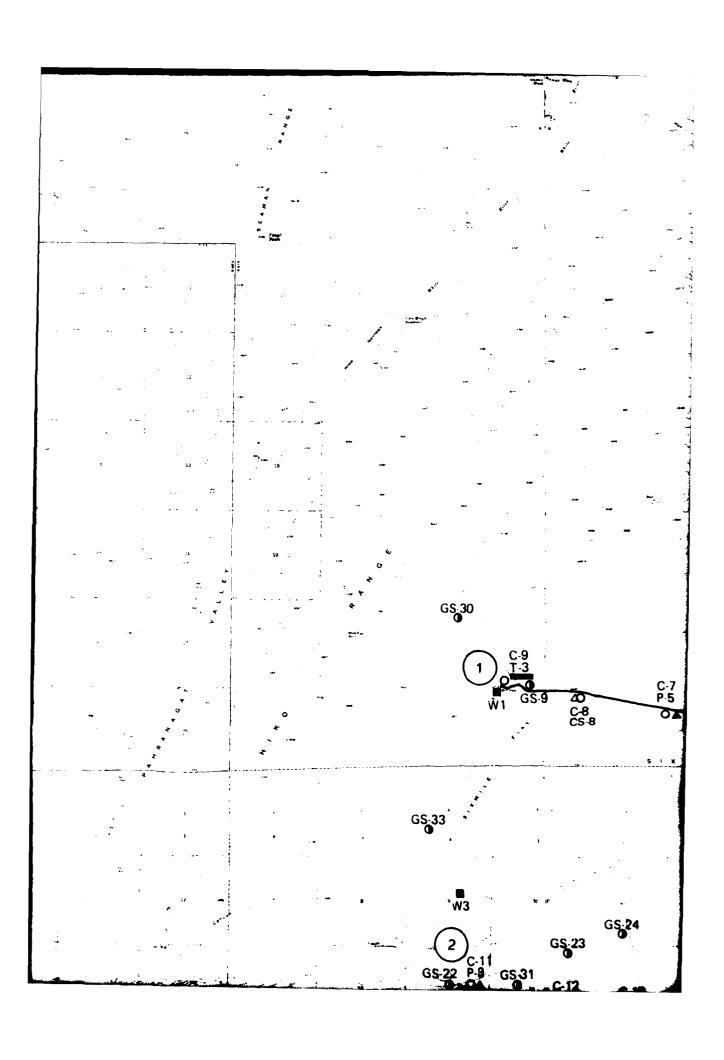
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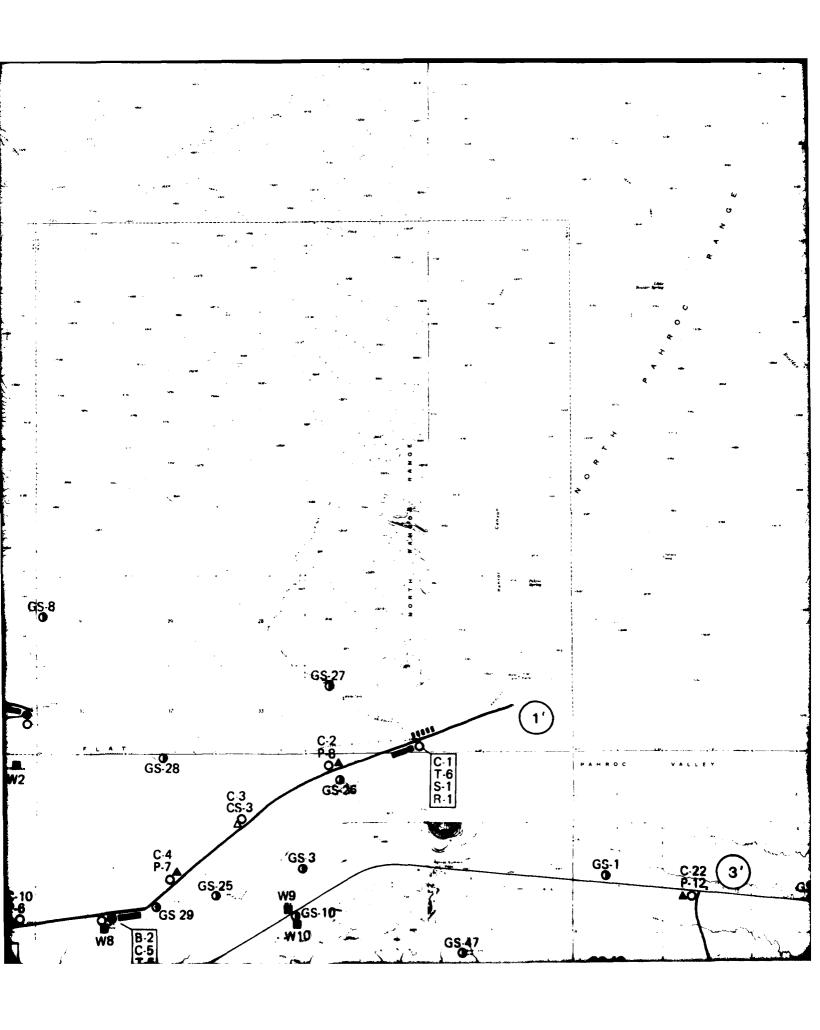
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	DEG	MIN	DEG	MIN	N(KM)	E(KM)
					~~~~~~	
TEST P	ITS					
				6. 51	4152. 59	667. 19
		31. 92				
PA- PO				8. 39		
PA- PO						672. 29
PA- PO		36. <i>71</i>		6. 00 5. 03		667. 62 669. 14
PA- PO	0 J/	36. 91	110	2 17	4163. 67	
PA- PO	, 3, 8 37	38 05	115	1. 20		
		35. 11			4161. 59	682. 56
		34. 15			4159.77	
					4157. 41 4164. 72	678. 66
PA- P1	2 37	36. 82	114	56. 74	4164. 72	681. 32
TRENCH	SIT	ES				
					4151. 46	668. 26
		35. 50				
PA- TO						664. 66
					4167. 76	
PA- 10					4164.08	
PA- 10	0 3/	30. 47	112	U. 13	4167. 34	676. 28
WATER	WELL	SITES				
PA- WO	1 37	39. 01	115	8. 03	4168. 43	664. 63
PA- WO	2 37	38. 07	115	5. 07	4166. 79	669. 02
PA- WO				8. 49		664. 03
PA- WO				7. 49	4162. 58	665. 5 5
PA- WO				7. 83		
PA- WO				6. 03	4161.38	667. 72
PA- WO				8. 97	4159. 26 4163. 89 4164. 18	663.43
PA- WO				4. 05	4163.89 4164.18	6/0.0/
PA- WI					4164. 03	
PA- W1			115	8. 82	4154.87	663. 73
PA- W1			115	8. 76	4153. 28	663. 85

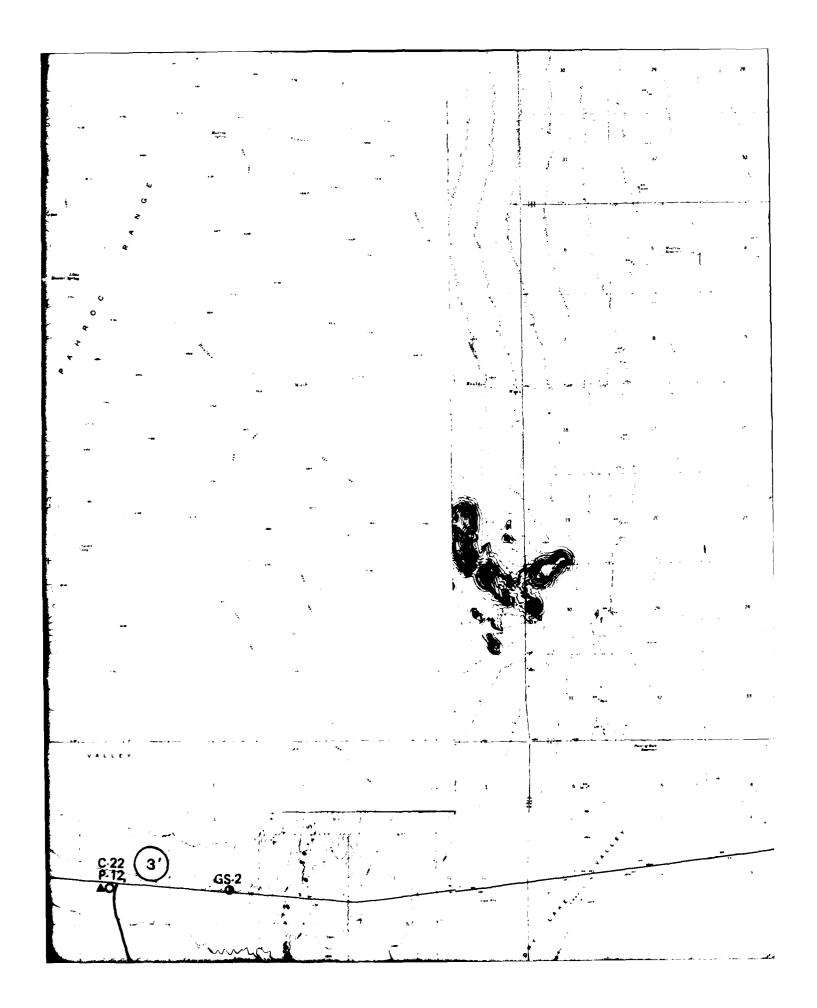


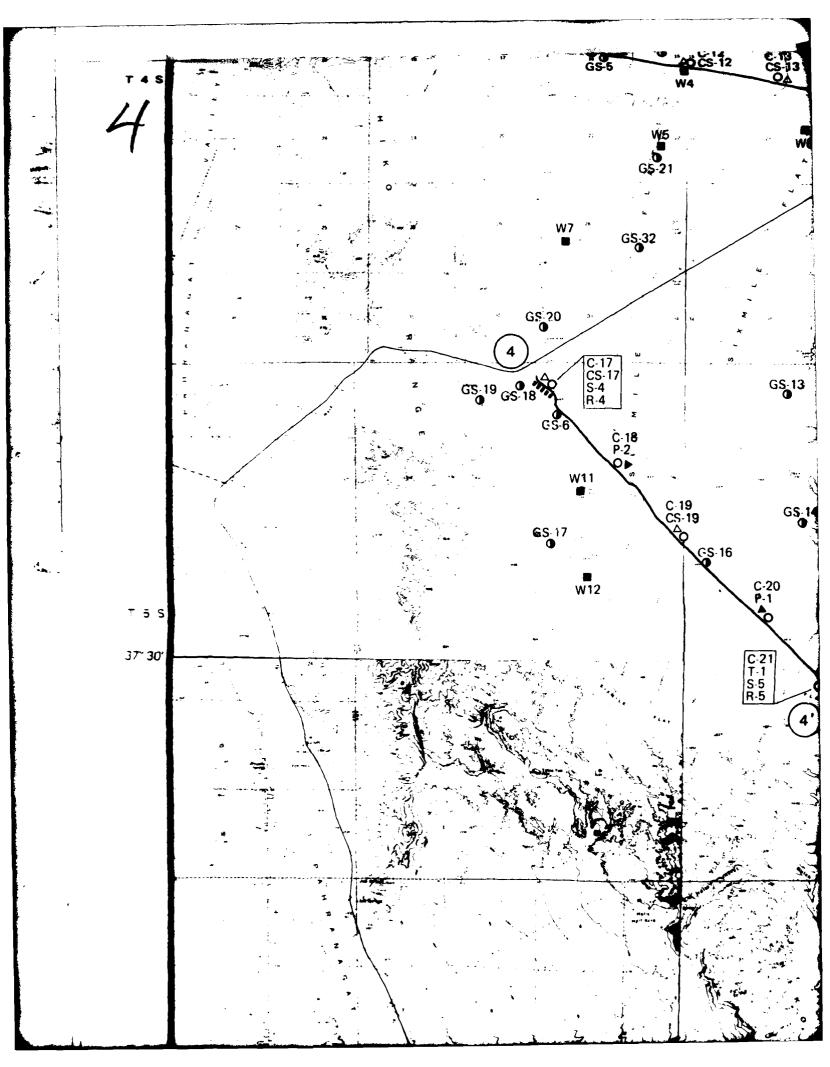
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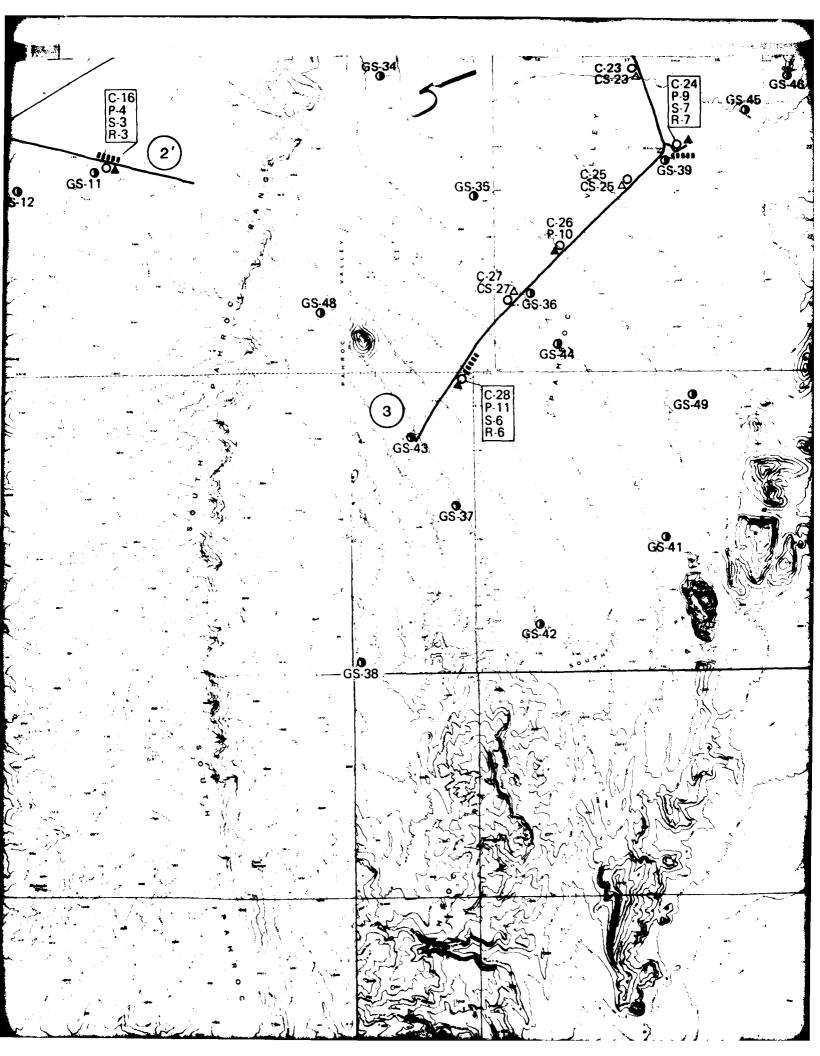
GEODETIC AND UTM COORDINATES OF ACTIVITY LOCATIONS PAHROC VALLEY, NEVADA PAGE 4 OF 4

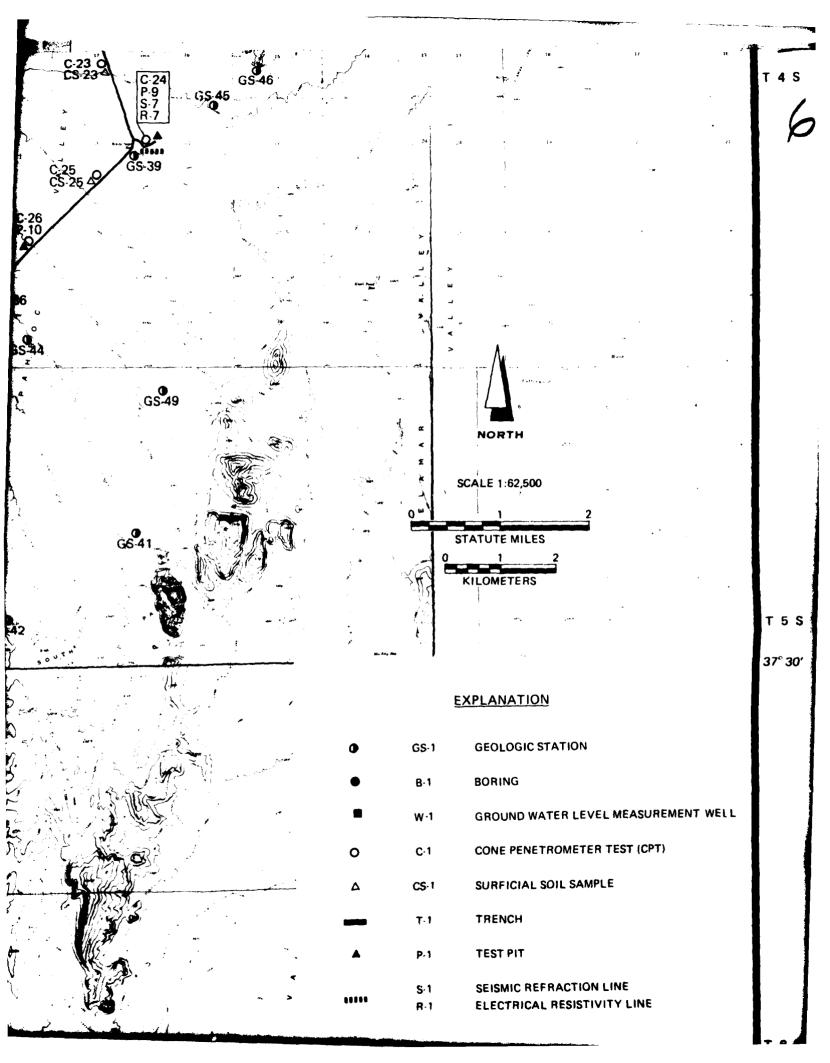


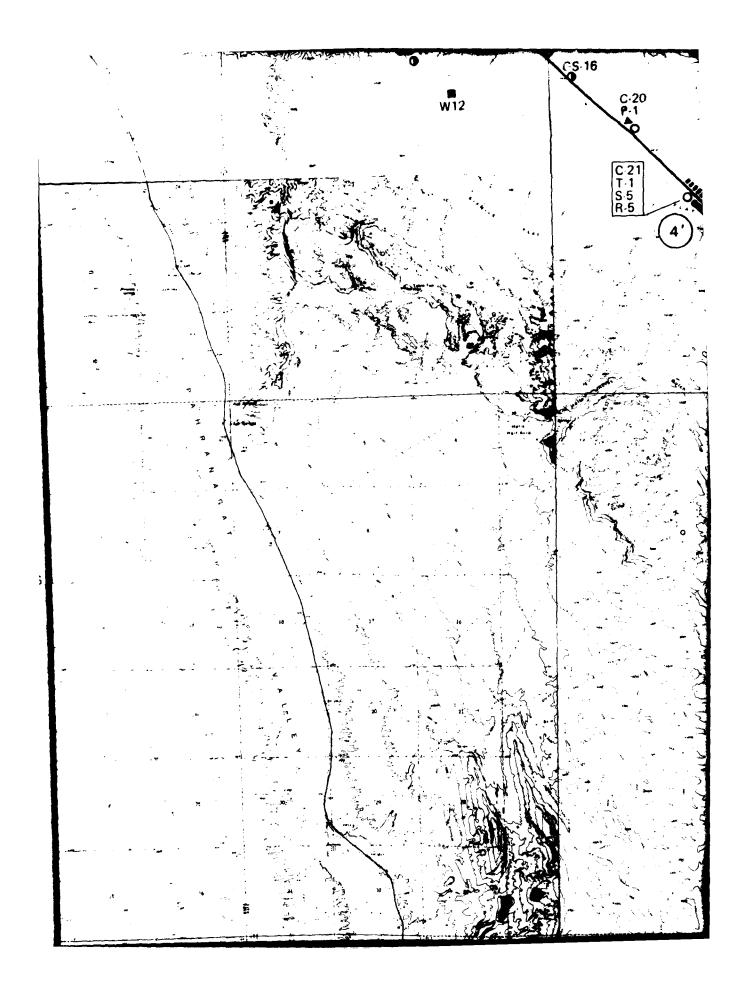


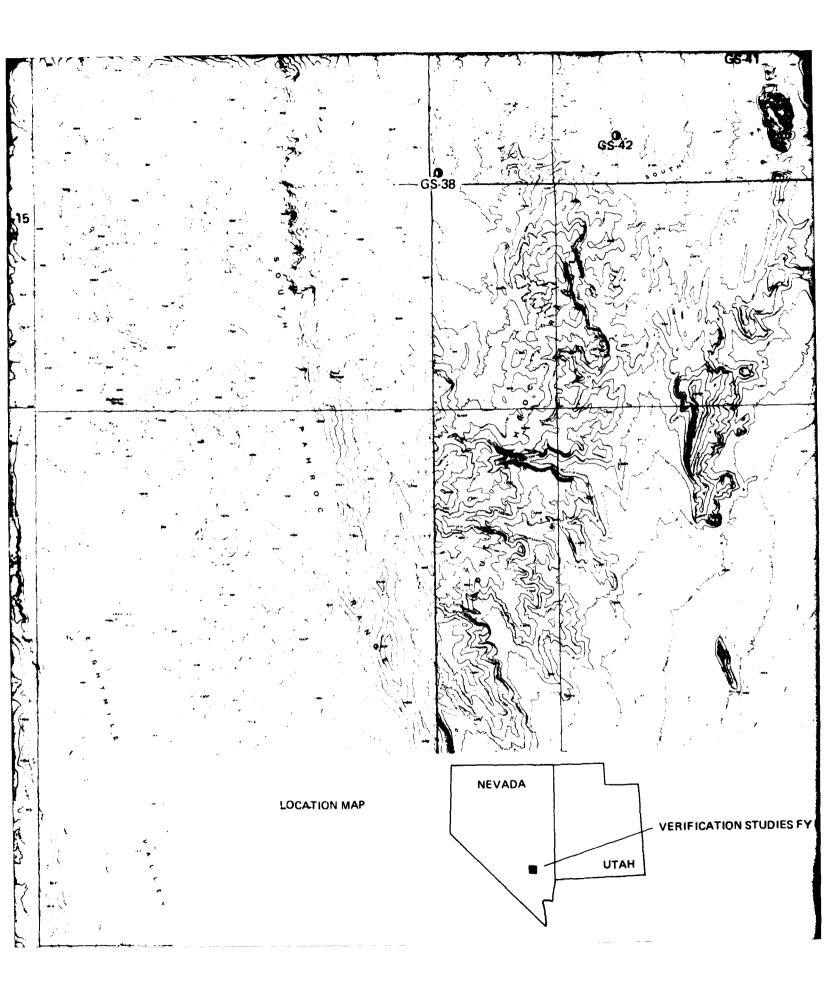


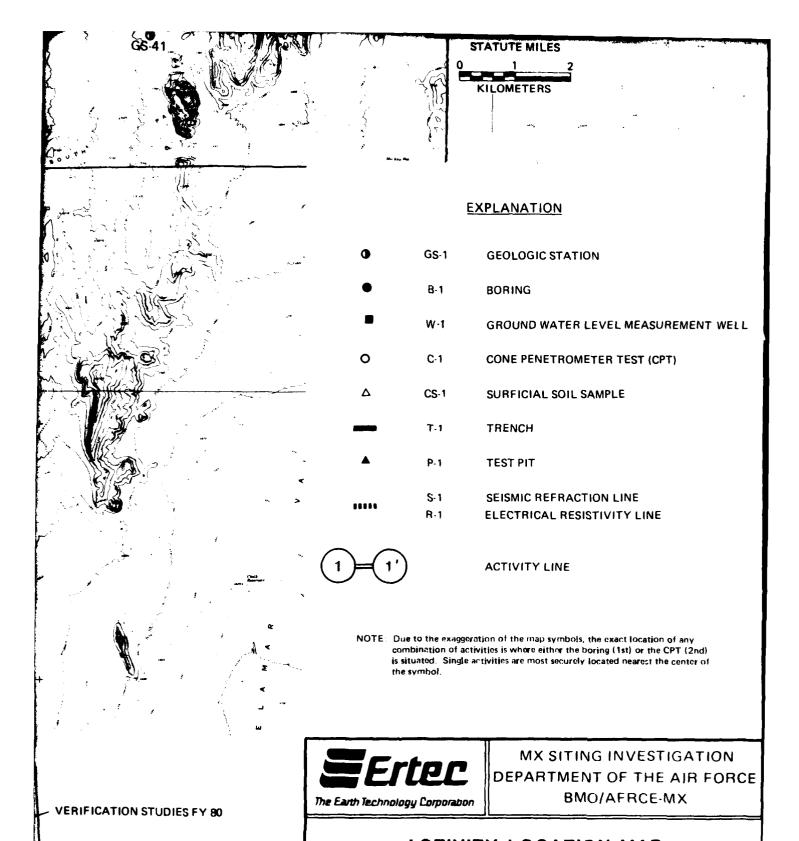












ACTIVITY LOCATION MAP PAHROC VALLEY, NEVADA

30 JUN 81

DRAWING II-1-1

2.0 GEOLOGIC STATION DATA

Explanation: Geologic stations were established at selected locations throughout the valley at which detailed descriptions of surficial basin-fill deposits or rock were recorded. An example of the field data sheet is shown in Figure II-2-1. All data taken on surficial basin-fill units at the geologic stations are listed in Table II-2-2, and an explanation of the column headings in the table is given below. At stations where rock descriptions were made, only geologic unit designations are listed. A general explanation of all geologic unit symbols used in Verification studies is included at the end of this section.

Column Heading Table II-2-2	Explanation
Station Number	Geologic stations are numbered sequentially. (e.g., NPAG001; N= Nevada-Utah Study Area; PA= Valley abbreviation [Pahroc]; G= Geology Station).
Geol. Unit	Generalized mapped geomorphic unit (see explanation below). The grain-size designations (s, g, and f) indicate sand, gravel, and fines, respectively.
MPS (mm)	Average Maximum Particle Size in millimeters.
Grain Size (%B, %C, %G, %S, %F)	Estimated particle size distribution using the Unified Soil Classification System. Percentages of boulders (%B) and cobbles (%C) are based on the entire deposit, whereas percentages of gravel (%G), sand (%S), and fines (%F) are taken only on the fraction composed of particles less than 3 inches (76 mm) in diameter. Note: The symbol Ø (occasional) indicates between 1 and 5 percent; zero indicates 0 to 1 percent.

Laboratory analyses of selected soil samples using the Unified Soil Classification System.

USCS Soil class according to the Unified Soil Class-ification System.

Munsell Color Soil color based on standard Munsell Soil Color Charts.

Source Rock Rock types of coarse clasts (gravel) listed in Types order of abundance.

Physical Data listed in columns 6 through 15 address specific soil properties. These are listed below in parentheses following the column heading number and are also listed at the bottom of Table II-2-1. Data are coded with each numerical entry referring to a specific soil condition as listed below.

- 6 (Grain Shape) 1) Angular, 2) Subangular, 3) Subrounded, 4) Rounded, 5) Well rounded
- 7 (Moisture 1) Dry, 2) Slightly Moist, 3) Moist, 4) Very Content) Moist, 5) Wet
- 8 (Plasticity 1) None, 2) Low, 3) Medium, 4) High
 of Fines)
- 9 (Consistency) Coarse-grained: 1) Very Loose, 2) Loose, 3) Medium Dense, 4) Dense, 5) Very Dense

Fine-grained: 1)Soft, 2) Firm, 3) Stiff,
4) Hard

- 10 (Structure)
 1) Non-stratified, 2) Stratified, tabular,
 3) Stratified, other (lensed, cross bedded, discontinuous beds)
- 11 (Cementation- 1) None, 2) Weak, 3) Moderate, 4) Strong
 Induration)
- 12 (Depth to Depth to layer (in centimeters) exhibiting Cemented cementation-induration described in Column 11 (above)
- 13 (Weathering 1) Fresh, 2) Slight, 3) Moderate, 4) Very of clasts)

14 (Soil 1) None (A-C profile), 2) Poor (incipient B-horizon), 3) Well (prominant B-horizon) Development)

15 (Caliche 1) None, 2) Stage I, 3) Stage II, 4) Stage Development) III, 5) Stage IV

Terrain Terrain information at the data location is broken into the following categories:

Drainage Depth Average depth of drainages (in feet) (ft)

Drainage Width Average width of drainages (in feet) (ft)

Slope (%) Average slope of ground surface (in percent grade)

Sample Number of samples taken

GENERALIZED GEOLOGIC UNITS

Explanation

Surficial Basin-fill Units

- Al Younger Fluvial Deposits Major recent stream channel and floodplain deposits.
- A2 Older Fluvial Deposits Older incised stream channel and floodplain deposits in elevated terraces bordering major recent drainages. Note: Not mapped in Delamar Valley.
- A3 Eolian Deposits Windblown deposits of sand occurring as either thin sheets (A3s) or dunes (A3d).
- A4 Playa and Lacustrine Deposits Deposits occurring in modern, active playas (A4) or in either inactive playas or older lake beds and abandoned shorelines associated with extinct lakes (A4o).
- As Alluvial Fan Deposits Alluvial deposits consisting of debris flow and water-laid alluvium near mountain fronts, grading into predominantly water-laid alluvium deposited in shifting distributary channels near the basin center. Younger (A5y), intermediate (A5i), and older (A5o) alluvial fans are differentiated by surface soil development, terrain conditions, and present depositional/erosional environment.

Grain sizes of these deposits (except A3 deposits, which are exclusively sandy) are indicated by a single letter (f, s, or g) following the geologic unit symbol. These letters indicate the predominant grain size and range of soil types according to the Unified Soil Classification System.

- f fine-grained clays and silts (ML, CL, MH, CH)
- s sands (SP, SW, SM, SC)
- g gravels (GP, GW, GM, GC)

ROCK UNITS

- I Igneous (undifferentiated). Rocks formed by solidification of a molten or partially molten mass.
 - Il Intrusive Plutonic rocks formed by solidification of molten material beneath the surface (e.g., granite, granodiorite, diorite, gabbro).
 - I2 Extrusive (intermediate and acidic) Volcanic rocks of intermediate and acidic compositon formed by solidification of molten material at or near the surface, (e.g., rhyolite, latite, dacite, andesite).
 - I3 Extrusive (basic) Volcanic rocks of basic composition, generally formed by solidification of molten materials at or near the surface (e.g., basalt).
 - I4 Extrusive (pyroclastic) Rocks formed by accumulation of volcanic ejecta (e.g., ash, tuff, welded tuff, agglomerate).
- S Sedimentary (undifferentiated) Rocks formed by accumulation of clastic solids, organic solids, and/or chemically precipitated minerals.
 - S1 Arenaceous and/or Siliceous Rocks Composed of sandsize particles (e.g., sandstone, orthoguartzite) or of cryptocrystalline silica (e.g., opal, chert).
 - S2 Carbonate Rocks Composed predominantly of calcium carbonate detritus or chemical precipitates (e.g., limestone, dolomite, chalk).

- S3 Argillaceous Rocks Composed of clay and silt-sized particles (e.g., siltstone, shale, claystone).
- S4 Evaporite Rocks Precipitated from solution as a result of evaporation (e.g., halite, gypsum, anhydrite, sylvite).
- S5 Coarse Clastic Rocks Composed of gravel sized or larger clasts (e.g., conglomerate, breccia).
- M Metamorphic (undifferentiated) Rocks formed through recrystallization in the solid state of preexisting rocks by heat and pressure (e.g., gneiss, schist, hornfels, metaquartzite).



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FIGURE II-2-1

			<u> </u>	
TERRA	AIN			
16. A	Average Drainage Depth (ft)	76		y
17.	Average Drainage Width (ft)		1 100	
18. S	Slope (percent) - field and/or topo	map measureme	A A	T B A
SURFA	ACE FEATURES			FIELD
19. P	Pit Depth (cm)			
20. 1	Thickness of Vesicular Silt (cm)		<u> </u>	
21. D	Desert Pavement Development (None, Poor, Moderate, Well)			
22. F	Patina Development (None, Moderate, Well)	· · · · · · · · · · · · · · · · · · ·		
COMME	ENTS			
COMME	ENTS			
COMME				
ROCK	DESCRIPTIONS			
ROCK 23. F	DESCRIPTIONS Rock Type/Formation			
ROCK 23. F	DESCRIPTIONS			
ROCK 23. F 24. C	DESCRIPTIONS Rock Type/Formation	e		
ROCK 23. F 24. C	DESCRIPTIONS Rock Type/Formation Color, Grain size, Hardness, Textur	e		

27. Secondary Alteration/Mineralization ____



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FIELD DATA SHEET PAGE 2 OF 2

30 JUN 81

FIGURE 13-2-1

	_		:								S	ü	1 1		٤	s c	R	PT	1 0 N							<u>-</u>			1	T E	R	RA	IN	•	
STATION NUMBER	1	UNIT	3 1991	X	X	C :	KC.		×Γ		USCS		ü	KSELL JLUK		RO	SOU	RCE TYPES	6									15	: 10				GLOPE (X)		MPLE
PAGS001	1	A5YS	1 30	9	,	0	1	53	10		co			west a		~			2	3	2	2	1	1		2	1	1	1				2		1
PAGS002							3		5		SP 5	•	7.5	YR4/	4 I	2			2	3	1	2	1	2	63	2	2	•		1.0		3.0	2		0
PAGS003						?		23	5		S E	n	7.5	57K4/	4 1	2			2	3	1	3	1	2	30	2	1	4					3	•	1
PAGS004 PAGS005								27 67	3		Sř.			YK5/		_			2		1	2	1	2	76	2	1	2		0.0		3.0	2		0
PAG5005											ين هي)YK4/)YK4/					2	3	1	2	2	1	**	2	2	2		1.0		7.0	3	:	ĭ
PAGS007									5		SPIS										1	ž	•	2	21	3	3	4		2.0		3.0	3	:	ò
PAGS000					1			86	4		SF			YR4/							i	-	i	2	40	3	2	4	-	2.0		3.0	2	:	ĭ
PAGS009					, 1			60	15		SM)YR5/						3		3	2	3	30	2	2	4		3.0		6.0	3	:	۸
PAGS010							3				5F - S						-			ĭ	1	2	3	1	30	ź	í	ī		3.0		B. U	3	:	ĭ
PAGS011			;	•			-	٠,		-				,,,,,,,	•	•			-	•	•	-	•	•		-	•	•	:				-		;
PAGS012				C		^	4	E 1	15	*			10.0	YR4/	4				2	1	2	2	1	3	25	2	1	4		5.0	14	5.0	5	i	i
PAGS013								εī	15					YR4/						î		2	ī	2	34	2		4		5.0			3		ī
PAGS014								75	- 5		5P-9					4				ì	i	-	ŝ	•	•		i	ī		<u> </u>			•	ī	ō
PAGS015					-				_						_				_	-	-		_			_	_	-	3						1
PA65016	:	ASYS	: 10	9		9	Ç	90	10		SF-S	ж.	10.0	YR3/	6				2	1	1	2	1	1		2	1	1					4		ō
PAGS017	1	ASTR	: 210	٠,	, ,	9	40	25	35		SH				S	2			3	1	3	3	1	2	10	2	1	3	2	3.0		7.0	6	•	0
PAG6018	1	A5Y5	2 3.3	C		0	0	75	5		SP-S	h :	10.0	YR4/	4				2	1	1	3	1	.5	45	2	1	4		23.0	- 5	0.0	5	2	1
PAGS019			1																										2						1
PAG5020					,			30	15		SM		10.0	YR5/	4 I	4				1		4	1	.3	10	2	1	4		5.0	33	0.0			0
PAGS021					, ,	2	1	97	12	*	on s	ň.	10.0	3YK3/	4				2	1	1	3	1	3	30	2	2	3	2				2		1
PAGS022																																		1	1
PAGS023								٠	- 3		SF			37K3/						1		3		1			1	2		3.0	5	0.0	1	1	1
PAGS024					,				20					YR3/			2					3	1	2	43		1	3					2	1	0
PAGS025				C	•	0	15	73	12	*	SP-9	m .	10.0	DYK4/	4 I	4			2	1	1	3	1	3	38	2	2	2	2	0.0	,	3.0	3		1
PAG5026			!	_													_			_	_		_	_			_	_	3		_		_		1
PAGS027						- 1		45		٠				JAK6					2	1		3	1	3	27	2	1	•		5.0		0.0	2	•	1
PAGS028 PAGS029						5 3		7.7	13							2 1	٠ ٤.	3 51		1	1	3	1	1		2	1	2		1.0		3.0	2	:	9
PAGS030									ت ن		ଧୀ ଅନ- ଓ			/YK4/					2		i	2	1	3	42 36	2	1	2			~		3	:	ŏ
PAGS031								75			SM									i		ź	ì	1	30	2	1	3		5.0		5.0	5	:	ŏ
PAGS032								95			Se S					- 5	2 3/		ź	:	•	÷	:	.,	45	2	i	4		3.0	- 3	J.U		:	ŏ
PAGS033								30	=		Gr 5					9 C	•			i	i	3	i	5	~	2	î	2		20.0	-		1	:	ŏ
PAGS034						ő Ì		20	5		ು ಬಿ						•				î	3	î	ž	34	2	î	ž					2	:	ĭ
PAGS035						ó		27			Se S								2	3	2	3	i	2	20	5	2	3					ī	•	ī
PAGS036							ć	90			Si S									3	ž	ž	î	ī		2	ĩ	- 2					ī		ō
PAGS037				- 0) 1	Ō:	10	22	ទ		Siris								2	š	2	2	ī	3	29	3	2	4		3.0	3	0.0	3		Ō
PAGS038	2	ASIS	1 70	Ċ			5	90	15		SC			YR4/					2		3	3	1	3	44	3	3	4		2.0		7.0	Ā	¥	1
PAGS039	3	A1 5	, 3	7	٠.	9	n	74	21		ZM.			YK4/						3	2	3	3	1			1	2	8						1
PAGS040							0	20	ناز		والز		10.0	YR4/	4					1	2 -	3	1	1		2	1	2		2.0	;	3.0	1	1	1
PAGS041							Ξ.	577	40		ωín			/YK4/							3	4	2	3	39	2	2	3	3	5.0	1	3.0	4	3	٥
PAGS042			: 80	C	1	0	0	30	20		SM	- 1	10.0)YR5/	4 I	2			2	1	2	2	1	3	17	2	1	5		1.0	13	5.0	3	2	1
PAG6043			,			_													_		_	_				_		_	3	_			_	2	1
PAGS044							0	30	20		SM	1	10.0	YK5/	4					1		3	1	1			1	2		2.0		7.0	2		0
PAGS045			: 3	C	,	つ	•	60	30		üн.								2	1	1	3	1	1		2	1	5	3	2.0			3		1
PAGS046				_		_	_												_		_	_	_	_		_	_	_					_		1
PAGS047					1			55	15		٠i.			/Y144/						1		2	1	3	20	2	2	5		2.0		3.0	2		0
PA65048									10					YRS/		_				1		3	1	1		2	2	1		2.0		5.0	3		ō
PAGS049	,	4012	1 80	C	, ,	u	O	100	Ü		SP)YI:37					2	1	1	3	1	4	30	2	2	5		7.0	10	0.0	4		0

EXPLANATION PHYSICAL PROPERTIES

61GRAIN SHAPE : 91CONSISTENCY :121DEPTH TO CEMENTED LAYER(CN):131CALICHE DEVELOPMENT 21M01STURE CONTENT :10:CURROLURE :131MEATHERING OF CLASTS :NOTE: 0-0CHASTONM:(1-5X) 81PLASTICITY OF FIRES :11:CEMENTATION-INDURATION :141SOIL PROFILE DEVELOPMENT :NOTE: 3-LAB DATA



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GEOLOGIC STATION DATA PAHROC VALLEY, NEVADA

30 JUN 81

TABLE II-2-1

3.0 GROUND-WATER DATA

Explanation: Existing ground-water data in Pahroc Valley were collected from all available sources. These data were updated where possible from measurements taken during Ertec field operations, and all data are shown in Table II-3-1. Locations of water wells and boreholes in which water-level measurements were available are shown in Drawing II-1-1. Well numbers listed in the left hand column of Table II-3-1 refer to well locations shown in Drawing II-1-1. Actual well numbers giving location, according to the Bureau of Land Management Land Survey System, are shown in the second column.

Water levels generally refer to the static ground-water table in the unconfined basin-fill aquifer. Perched conditions or levels in artesian aquifers are noted where known.

				W			
WELL NO.	WELL LOCATION NUMBER* (Twp-Rge-Sec)	ELEVATION OF GROUND SURFACE FEET (METERS) ABOVE M.S.L.	DEPTH OF WELL FEET (METERS)	DEPTH BELOW GROUND SURFACE- FEET (METERS)	DATE	ELEVATION— FEET (METERS) ABOVE M.S.L.	REFERENCES*/
W1	3S/61E-34bb	4713 (1437)	>500 (152)	dry	6-80	4213 (1284)	2
W2	4S/61E-1aa	4520 (1378)	500 (152)	dry	6-80	< 4020 (1226)	2
W3	4S/61E-9ac	4460 (1372)	300 (92)	dry	10-65	< 4160 (1268)	3
W4	4S/61E-15db	4320 (1317)		670 (204)	2-77	3650 (1113)	1, 4
W5	4S/61E-22ca	4300 (1311)	310 (95)	dry	12-63	< 3990 (1216)	3
W6	4S/61E-23ad	4470 (1362)	160 (49)	dry	12-63	< 4310 (1314)	3
W7	4S/61E-28cac	4230 (1290)	1314 (401)	595	12-68	3635 (1108)	. 3
W8	4S/62E-7dd	4640 (1415)	104 (32)	dry	6-80	< 4536 (1383)	2
W9	4S/62E-9dd1	4900 (1494)	410 (125)	dry	10-65	< 4490 (1369)	3
W10	4S/62E-9dd2	4920 (1500)	240 (73)	dry	10-65	< 4680 (1429)	3
W11	5S/61E-9ca	4410 (1345)	30 (9)	dry	6-80	<4380 (1336)	2, 3
W12	5S/61E-16bd	4425 (1349)	30 (9)	dry	6-80	< 4395 (1340)	2, 3
							

*MOUNT DIABLO BASELINE AND MERIDIAN

- •• REFERENCES:
 - 1. EAKIN, 1983
 - 2. FUGRO NATIONAL MEASUREMENT (1980)
 - 3. NEVADA STATE ENGINEERS WELL LOGS
 - 4. U.S.G.S. WELL INFORMATION PRINTOUT



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GROUND-WATER DATA PAHROC VALLEY, NEVADA

30 JUN 81

TABLE II-3-1

4.0 SEISMIC REFRACTION DATA

Explanation: Each figure shows seismic wave travel times plotted versus surface distance between the energy source (shot) and the detector (geophone) for a single seismic line. Distances are measured along the line from geophone number 1 which is designated as zero distance. Distances to the right (on the paper) of geophone 1 are positive. The direction arrow gives the approximate direction of the geophone array from geophone 1 to geophone 24.

Travel Time Versus Distance Graph (Upper Half of Figure)

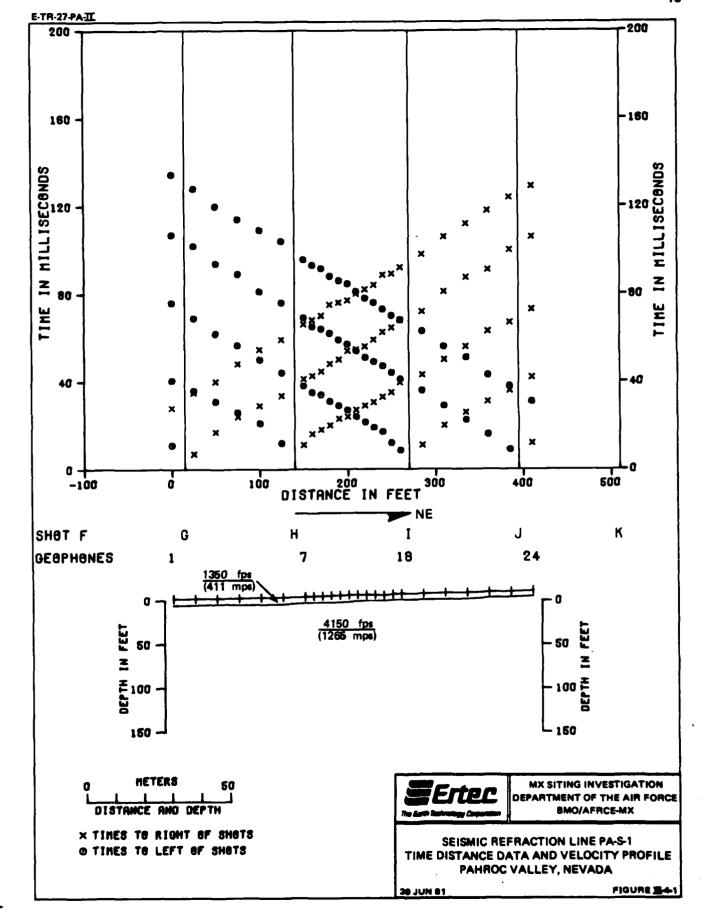
On this graph, the abscissa represents distance; the ordinate, time. The six vertical lines represent the locations of shots (designated as F, G, H, I, J, and K). The symbol "X" denotes travel times at geophones that were located to the right of a shot. The symbol, 0, denotes travel times that were located to the left of shots.

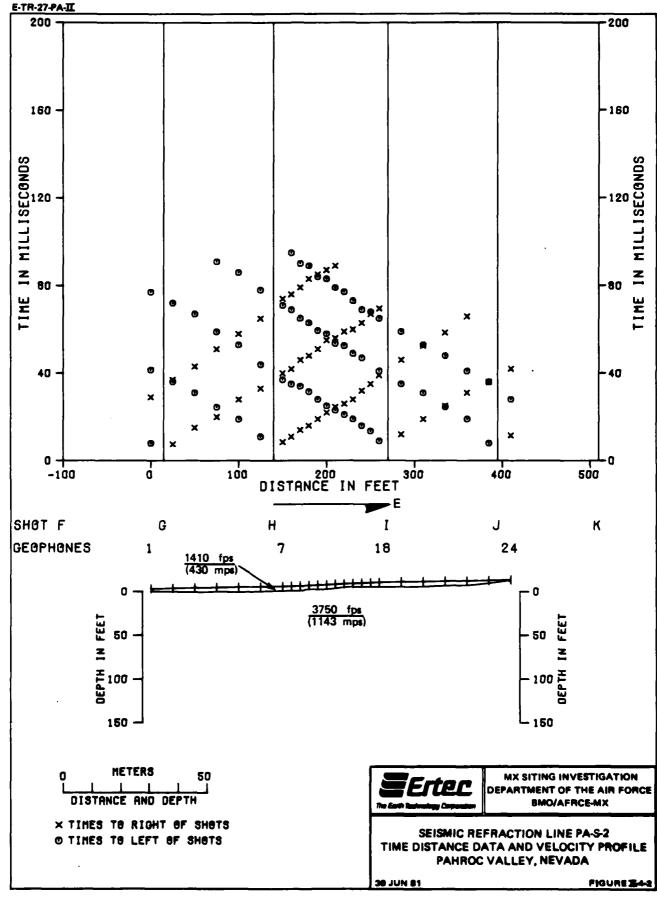
Velocity Cross Section (Lower Half of Figure)

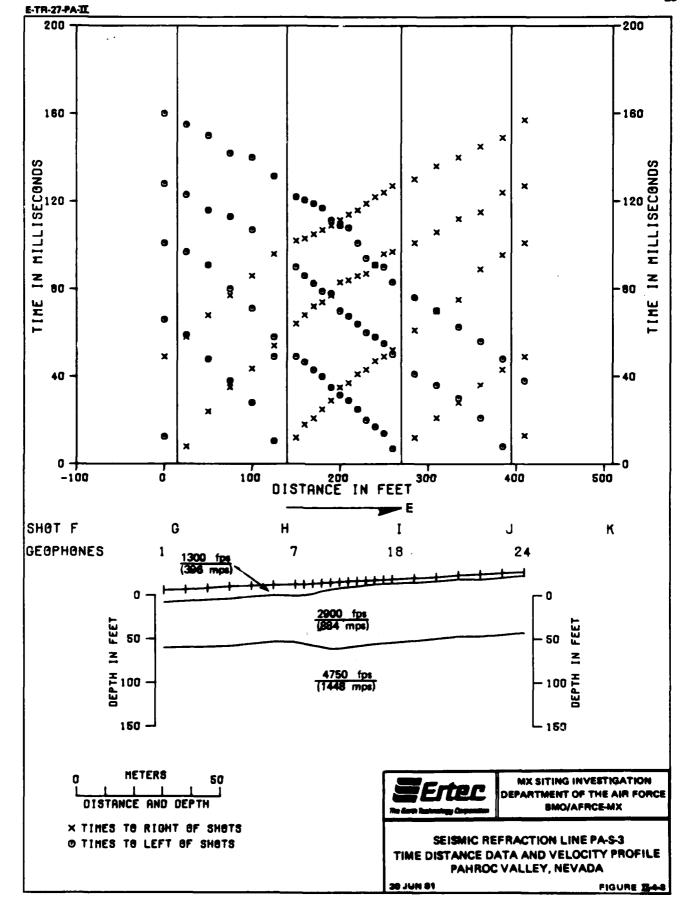
This is an interpreted velocity cross section beneath the seismic line. The top line represents the ground-surface profile. The short vertical lines crossing the top line mark the geophone positions. The depth scale is plotted relative to a point on the line which was arbitrarily chosen as "zero elevation" at the time the line was surveyed. The additional lines across the cross section represent the interpreted boundaries between layers of material with different compressional wave velocities. These boundaries are commonly called "refractors."

E Ertec

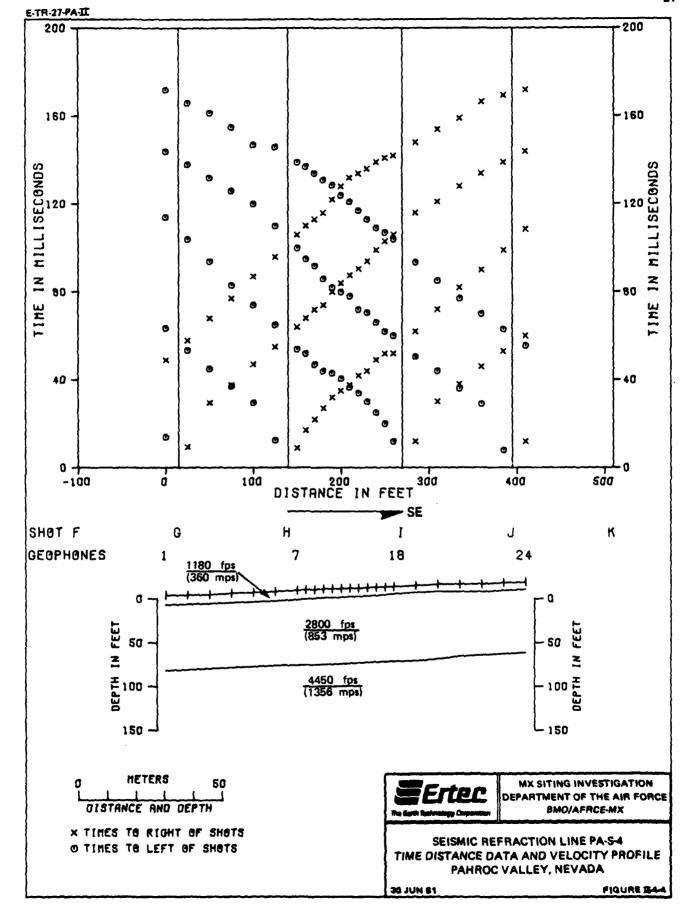
The velocity interpreted to be representative of each layer is shown.





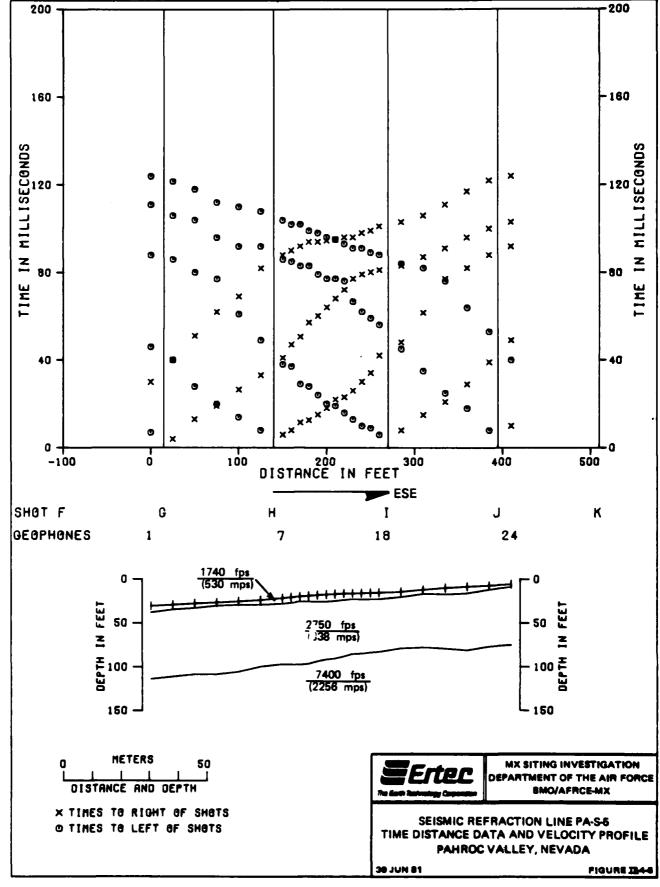


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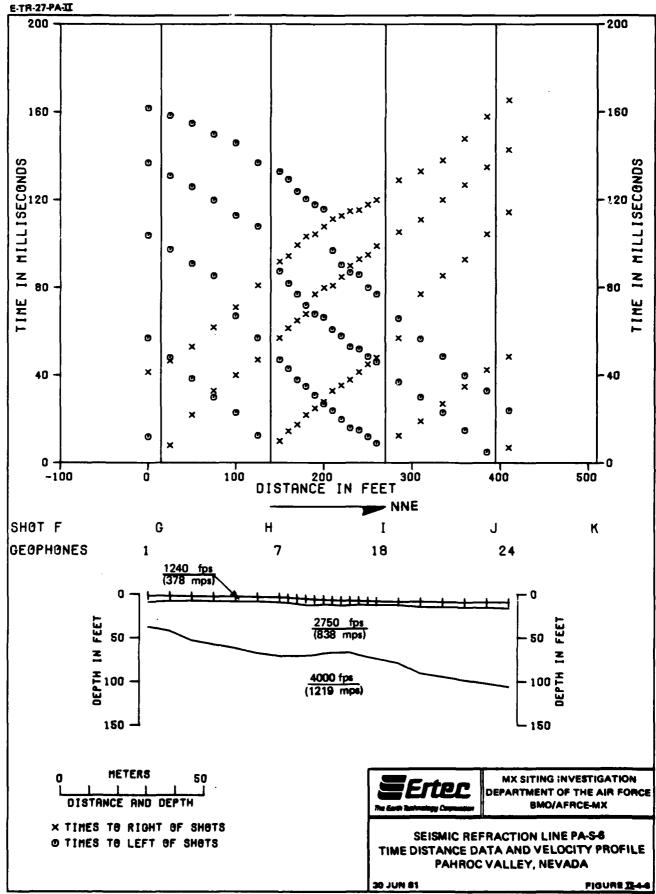


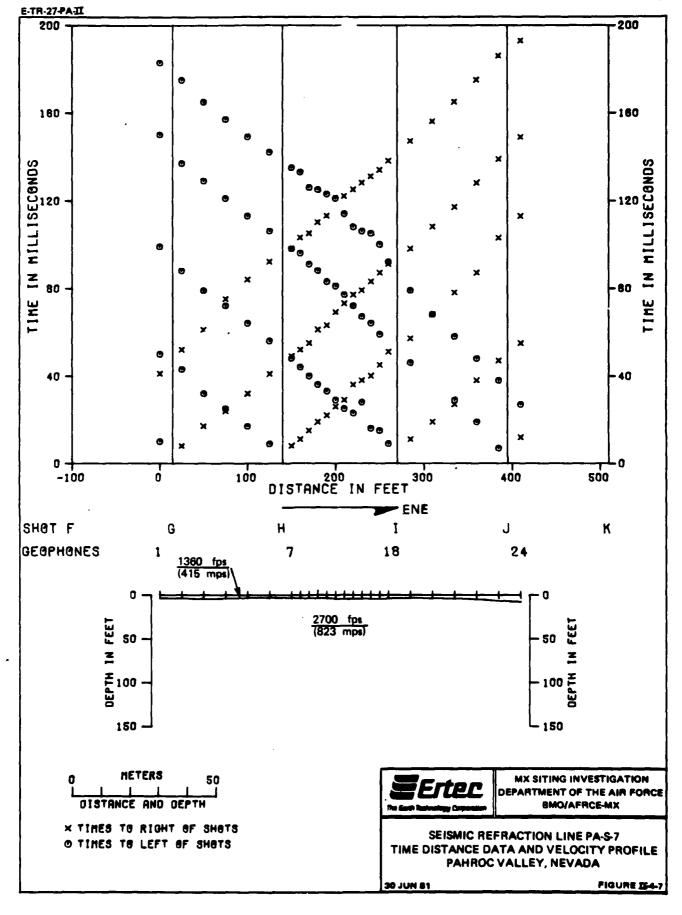
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- 1



E-TR-27-PAJI





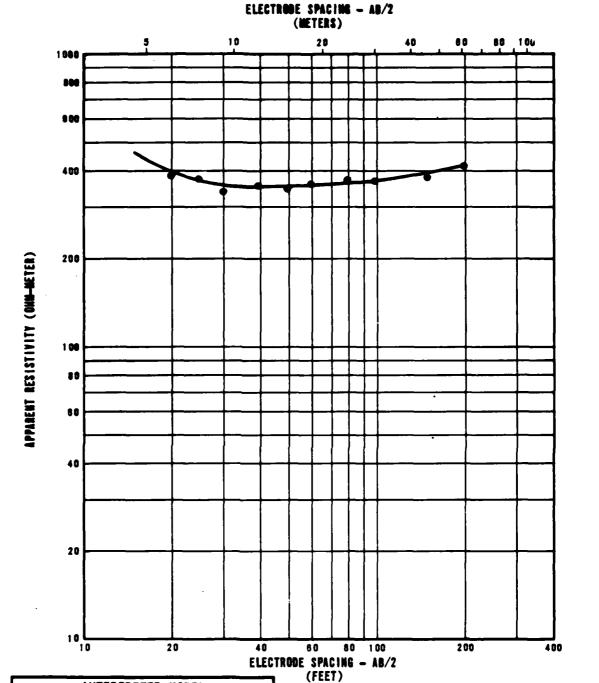
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5.0 ELECTRICAL RESISTIVITY DATA

Explanation: Each figure in this section presents the data obtained from a resistivity sounding and a tabulated model of resistivity layers that would produce a curve similar to the observed curve.

The upper portion of the figures is a graph in which measured apparent resistivity values in ohm-meters are plotted versus one-half the distance between the current electrodes.

The interpreted model tabulated at the bottom of the page shows a combination of true resistivity layers and thicknesses obtained by matching theoretical curves to the field curve.



	INTERPRE	TED MODEL
LAYE	R DEPTH	RESISTIVITY VALUES
FEET	METERS	OHM-METER
0	0	640
5	2	360
77	23	490

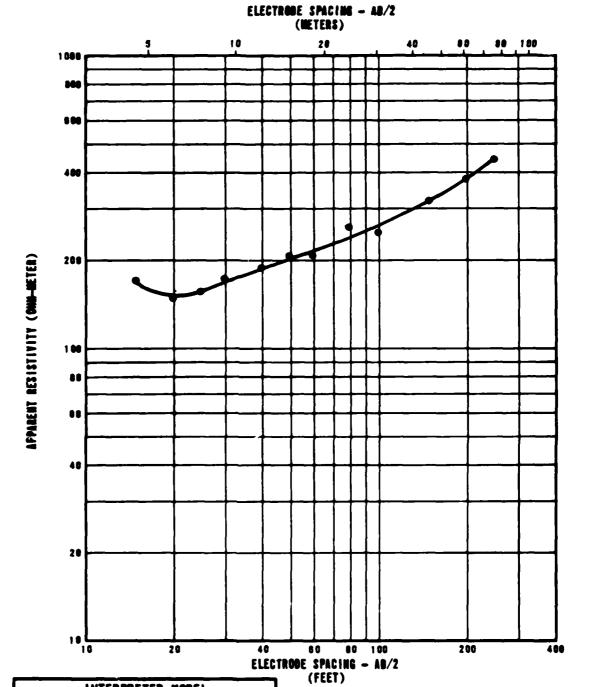


RESISTIVITY SOUNDING PA-R-1 SOUNDING CURVE AND INTERPRETATION PAHROC VALLEY, NEVADA

30 JUN 81

FIGURE 3-6-1

USAF-15



_	INTERPRE	TED MODEL
LAYE	LAYER DEPTH EET METERS 0 0 6 2 26 8	RESISTIVITY VALUES
FEET	METERS	OHM-METER
0	0	230
6	2	129
26	8	320
37	11	210
91	28	1200
	1	Ī

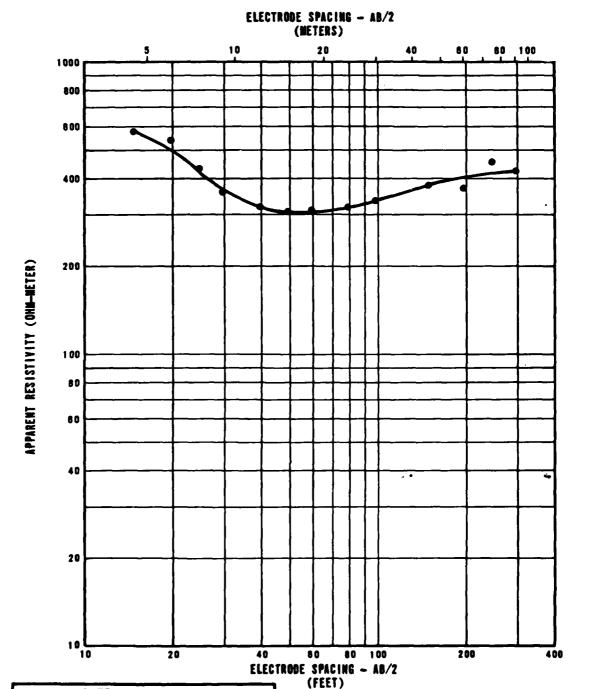


RESISTIVITY SOUNDING PA-R-2 SOUNDING CURVE AND INTERPRETATION PAHROC VALLEY, NEVADA

10 MUL 95

FIGURE IS-2

UBAF-18



	INTERPRE	TED MODEL
LAYE	R DEPTH	RESISTIVITY VALUES
FEET	METERS	OHM-METER
0	0	720
9	3	260
46	14	450
	T	

١



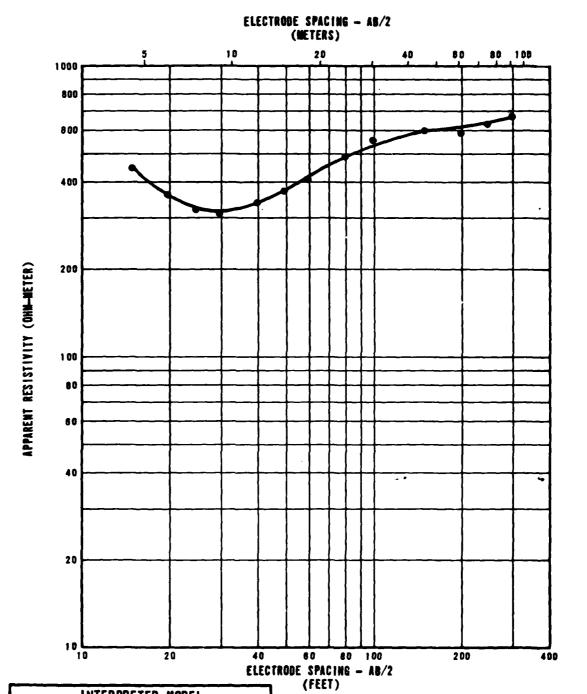
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RESISTIVITY SOUNDING PA-R-3 SOUNDING CURVE AND INTERPRETATION PAHROC VALLEY, NEVADA

30 JUN 81

FIGURE IL-3

98AF-15



	INTERPRE	TED MODEL
LAYE	DEPTH	RESISTIVITY VALUES
FEET	METERS	OHM-METER
0	0	720
7	2	160
20	6	810
79	24	480
149	45	860
	1	1

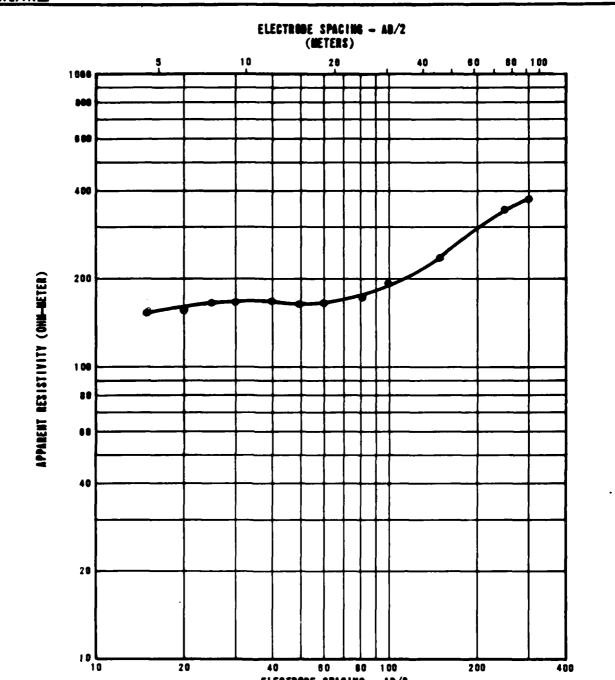


RESISTIVITY SOUNDING PA-R-4 SOUNDING CURVE AND INTERPRETATION PAHROC VALLEY, NEVADA

30 JUN 81

FIGURE 1154

VM F-11



(FEET)	TED MODEL	INTERPRE	
	RESISTIVITY VALUES	DEPTH	LAYER
	OHM-METER	METERS	FEET
	130	0	0
Erte	200	3	9
The Suich Restrictings Con	140	6	20
9501	730	22	71
RESI:			
300.10.111			

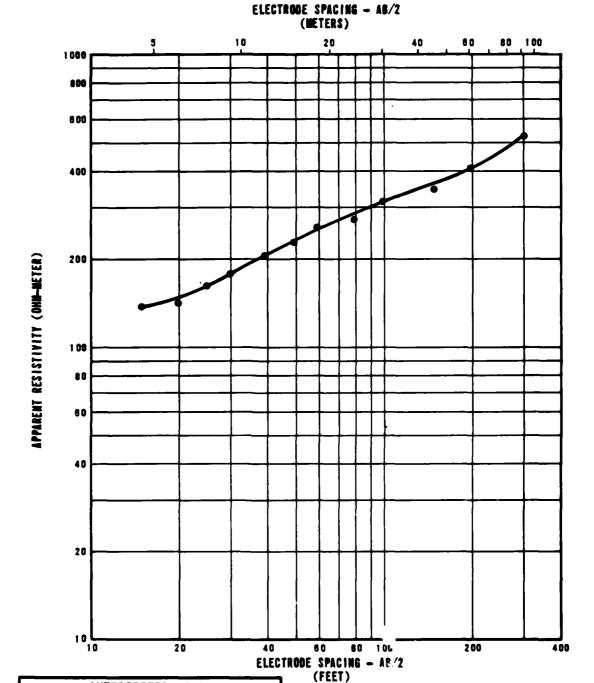


RESISTIVITY SOUNDING PA-R-5 SOUNDING CURVE AND INTERPRETATION PAHROC VALLEY, NEVADA

30 JUN 81

FIGURE IL-6

VMF-15



	INTERPRE	TED MODEL
LAYE	RDEPTH	RESISTIVITY VALUES
FEET	METERS	OHM-METER
0	0	130
20	6	470

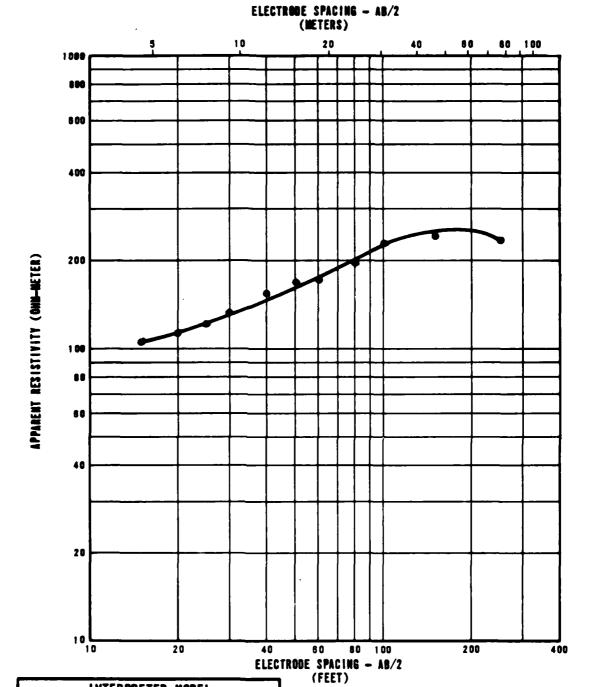


RESISTIVITY SOUNDING PA-R-6 SOUNDING CURVE AND INTERPRETATION PAHROC VALLEY, NEVADA

30 JUN 81

FIGURE 12-6

VBAF-18



	INTERPRE	TED MODEL
LAYE	R DEPTH	RESISTIVITY VALUES
FEET	METERS	OHM-METER
0	0	95
14	4	270
54	16	420
108	33	180



RESISTIVITY SOUNDING PA-R-7 SOUNDING CURVE AND INTERPRETATION PAHROC VALLEY, NEVADA

36 JUN 8

FIGURE IL

UMF-1

6.0 BORING LOGS

Explanation: All data from borings and trenches are presented on standard Ertec Western logs in Sections 6.0 and 7.0. Explanations of the column headings on the logs are as follows:

A. Designations - Borings and trenches are identified as follows:

PA-B-1

PA - abbreviation for the valley (e.g., PA-Pahroc)

B - abbreviation for activity (e.g., B-boring, T-trench, P-test pit)

1 - number of activity

- B. Sample Type Different sampling techniques were used and the symbols are explained at the bottom of the boring logs. For details of sampling techniques, see Section A5.0 of Appendix in Volume I (E-TR-27-PA-I). Horizontal lines, to scale, indicate the depth where sampling was attempted.
- C. Percent Recovery The numbers shown represent the ratio (in percent) of the soil sample recovered in the sampler to the full penetration of the sampler.
- D. N Value Corresponds to standard penetration resistance, which is number of blows required to drive a standard split-spoon sampler for the second and third of three 6-inch (15-cm) increments with a 140-pound (63.5 kg) hammer falling 30 inches (76 cm) (ASTM D 1586-67).
- E. Depth Corresponds to depth below ground surface in meters and feet.

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- F. Lithology Graphic representation of the soil and rock types.
- G. USCS Unified Soil Classification System symbols (see Table II-6-1 for complete details).
- H. Soil Description Except in cases where samples were classified based on laboratory test data, the descriptions are based on visual classification. The procedures outlined in ASTM D 2487-69, Classification of Soils for Engineering Purposes, and D 2488-69, Description of Soils (Visual-Manual Procedure), were followed. A solid line across the column indicates a change in strata at the depth shown.

Definitions of some of the terms and criteria to describe soils and conditions encountered during the exploration follow.

Gradation: A coarse-grained soil is well graded if it has a wide range in grain size and substantial amounts of most intermediate particle sizes.

Poorly graded indicates that the soil consists predominantly of one size (uniformly graded) or has a wide range of sizes with some intermediate sizes obviously missing (gap-graded).

Moisture: Dry - no feel of moisture-dry like powder

Slightly Moist - much less than optimum mois-

ture

Moist - near optimum moisture for soil

provides apparent cohesion

Very Moist - much greater than optimum

moisture

Wet - at or near saturation

Consistency: Consistency descriptions of coarse-grained soils (GW, GP, GM, GC, SW, SP, SM, SC) follow.

	(Excluding per	wys <u>1944</u> 1969 1991 1969 1994	Field Idealification Procedures particles larger than 3 in, and basing fractions on estimated weights)	ures Pasing fraction.	900	Symbols	Typical Names	Information Required for Describing Solis			Laboratory Classification Criteria	
	25	06 10 5 06 10 0 (898)	Wide range to amounts of sizes	in grain size and substantial of all intermediate particle	d substantisi	à	Well graded gravels, gravel- sand mixtures, little or no fines		acie di	.ew na :ewolk	$C_{ij} = \frac{D_{ij}}{D_{ij}}$ Greater than 4 $C_{0} = \frac{(D_{ij})^{3}}{D_{ij} \times D_{ij}}$ Between l and l	6 %
	o io ila latger i la svam asu sd	Clean (inil)	Predominantly with some	Predominantly one size or a range of sizes with some intermediate sizes missing	range of stacs sizes missing	3	Poorly graded gravels, gravel- sand mixtures, little or no fines	and gravel; maximum size; angularity, eurlace condition, and hardness of the coarse	#13 BB0	aller (fu es bs fo puirms	Not meeting all gradation requirements for GW	ents for GW
et lais dans :	40m 2011	st of stable stable	Nonplastic for cedures see	c fines (for identification pro- see ML below)	fication pro-	NO	Silty gravels, poorly graded gravel-sand-silt mixtures	and other periment descriptive information: and symbols in parentheses		poja W' 2C M' 2b M' 2b criou aur	Atterberg limits below Above "A" line, or PI less with than t	bove "A" line with P! between 4 and 7 are
300 men	eni . ni t se	isvanD ing angga) iuoma eng	Plastic fines (fo	es (for identification procedures, below)	a procedures,	ပ္ပ	Clayey gravels, poorly graded gravel-sand-clay maxives	ted soils add information, degrees		ines (frac d soijs ar 7, GP, SI 7, GC, S Mertine iual symi	above P.	requiring use of
Cosmo-sna then half then ho. visible to a	udig).	sbase a c or no (sam	Wide range in amounts of sizes	is grain tizes and substantial of all intermediate particle	d substantial	AS.	Well graded sands, gravelly sands, little or no fines	moitiure conditions and dhinage characteristics Example: Sity sand, gravelly: about 20%	ibi bisi 1si 18 lo 1seri	b M D Stantes M D % M D % M D %	$C_{\rm U} = \frac{D_{\rm MP}}{D_{\rm 10}}$ Greater than 6 $C_{\rm C} = \frac{(D_{\rm 20})^8}{D_{\rm 10} \times D_{\rm 40}}$ Between 1 and 3	3
noM nogen	mailen seve su al class	(1111)	Predominantly with some	anly one size or a range of sizes me intermediate sizes missing	range of sizes	\$	Poorly graded sands, gravelly sands, little or no fines	dero, angusta gravet perticus 1-in. maximum size; rounded and aubenquier sand grains control to fine about 15 % and		13% yeu 3% eu 2% eu beu	Not meeting all gradation requirements for SW	ents for SW
d sester	radis cion u No.4 s	creple creple ses aviry	Nonplastic fit cedures, s	Nonplassic fines (for identification pro- cedures, see ML below)	Acation pro-	75	Silty sands, poorly graded sand- silt mintures	plastic fines with low dry strength; well compacted and moss in place; alluvial sand;	Schuttra	Dending Do sieve Less th More t of % t	Allerberg limits below Above "A" line or Pliess than with 5	"A" line PI between nd 7 are
ne sel 1	18 1]	ng erqqe) emome	Plastic lines (fo	ts (for identification procedures, below)	a procedures.	ည	Clayey sands, poorly graded sand-clay mixtures	(MS)	Det	Jei Dei	Atterbers limits below required. "A" line with PI dual greater than 7	borderitus cases requiring use of dual symbols
noc	Identification	Procedures	on Fraction Sma	Smaller than No. 40 Sieve Size	40 Sieve Size				341			
1941 16 81 3843 3V	•		Dry Strength (crushing character- istics)	Distancy (reaction to shaking)	Toughness (consistency near plastic limit)				Bu ikji wapi	60 Comparing	Comparing solds of equal liquid limit	
2015 9	and clay	०६ वस्त्रा ।	None to	Quick to slow	None	Jų.	Inorganic siles and very fine sands, rock flour, silty or clayey fine sands with slight plasticity	Give typical name; indicate degree and character of plasticity, amount and maximum size of		\$ 	foughners und die strengft marene	
se beniere tatam to vau OOS.	ı bıl	t93i	Medium to high	None to very slow	Medium	ឌ	Inorganic ciays of low to medium plasticity, gravelly clays, sandy clays, silty clays, kan clays	condition, odour if any, local or geologic name, and other peri- aent descriptive information, and symbol in parenthees	sais ninri Plasfici <i>t</i>	e 2	ШM	
oM n			Shight to medium	Slow	Slight	70	Organic silts and organic silt-	For undisturbed soils add infor-		10	8	
adt an			Slight to medium	Slow to none	Slight to medium	ЖЖ	leorganic silts, micaccous or diatomaceous fine sandy or sitty soils, elastic silts	tion, consistency in undisturbed and remoulded states, moisture and drainage conditions	_	1	∭g	#8 8
)H	bas a bug bug	05_	High to very high	None	T GP	3	Inorganic clays of high plas- ticity, fat clays	Example:			Liquid limit	
	M		Medium to high	None to very slow	Slight to medium	МО	Organic clays of medium to high plasticity	Clayey sill, brown; slightly plastic; small percentage of		for labora	riasincity charry for laboratory classification of fine grained soils	ed soils
ž	Highly Organic S.	Soils	Readily ident	identified by colour, odour, feel and frequently by Abrous	our, odour,	-	Peat and other highly organic soils	root holes; firm and dry in place; loem; (ML)				
From Wag	From Wagner, 1957. • Boundary classifications.		Soils possessing characters	stics of two ga	roups are desig	mated by	combinations of group symbols. F	Cleaning of two groups are desimated by combinations of group tymbols. For example GW-CC, well graded gravel sand mature with clay binder.	avel-sand	mature with	lay binder.	

These procedures are to be performed on the minus No. 40 sieve size particles, appro-

Diseasory (Rescions to Abstrat):

After removing particles larger than No. 40 serve size, perpetr a pair of most seal with a volume of about one-half cube, irid. Add enough most seal with a volume of about one-half cube, irid. Add enough most seal with a volume of about one-half cube, irid. A dot enough waster in secsion you see that a particle of a serve is seller. A posture reaction consists of the appearance of water on the surface of the pair which changes to a livery constituent of water on the surface of the pair which changes to a livery constituent of water on the surface of the pair which is supposed to a papearance of water during abstrat and disest disappear from the surface, it po su stiffich and half in reacts or crumbles. The rapidity of appearance of water during thating and of its disappearance during very flac clean world more than the formation of the flact in a so of the control of the surface of water during thating and of its disappearance during very flac clean world now the surface of water during thating and of its disappearance during very flac clean world now the surface of water during thating and of its disappearance during a page.

Pagebeur (Consistency mear plassic limits). No. 40 steve size, a speciess of Alter removing particle larger instance is recolled to the consistency of any steve countries are consistency of some steve steve consistency of some steve the steve consistency to lose some steve the steve consistency of some steve in the steve constant is requisited to a smooth the steve consistency of some steve consistency of some steve the specimen is of the some steve constant is angularly reduced and the specimen suffers, death of the steve constant is angularly reduced and the specimen suffers, death of the steve constant is angularly reduced and the steve constant is the steve consistency of the thread may not some step steak them is and quick loss of constant constant and the step steak in the step in section of the steve of the thread may not below the speak time indicate the moral step constant so if the thread on the speak in the speak in section is set in section of the steve constant in the section of the steve of the thread on the speak in the speak in section is set of sets in the step step in the step of step of step in the step of step of step in the step of s



MX SITING INVESTIGATION **DEPARTMENT OF THE AIR FORCE BMO/AFRCE-MX**

UNIFIED SOIL CLASSIFICATION SYSTEM PAHROC VALLEY, NEVADA

30 JUN 81

TABLE II-0-1

0:	N Value
Consistency	(ASTM D 1586-67)
Very Loose	0 - 4
Loose	4 - 10
Medium Dense	10 - 30
Dense	30 - 50
Very Dense	>50

Consistency descriptions of fine-grained soils (ML, CL, MH, CH) are as follows:

	Consistency	Shear St (ksf) (k	Ξ.	Field Guide
	Very Soft	0.25	12	Sample with height equal to twice the diameter, sags under own weight
	Soft	0.25- 0.50	12 - 24	Can be squeezed between thumb and forefinger
	Firm	0.50- 1.00	24- 48	Can be molded easily with fingers
	Stiff	1.00-2.00	48- 96	Can be imprinted with slight pres- sure from fingers
	Very Stiff	2.00- 4.00	96- 192	Can be imprinted with considerable pressure from fingers
	Hard	over 4.00	over 192	Cannot be im- printed by fingers
Grain Shape:	Angular -	relative		sharp edges and e sides with aces.
	Subangular -			imilar to angular at rounded
	Subrounded -	sides bu		it nearly plane well-rounded es.

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Rounded - particles have smoothly curved sides and no edges. Containing calcium carbonate; presence of cal-Calcareous: cium carbonate is commonly identified on the basis of reaction with dilute hydrochloric acid. Soils cemented by calcium carbonate and/or Caliche other soluble minerals by upward-moving solutions. Degree of Cementation: (Stages of development of caliche profile) Stage Gravelly Soils Nongravelly Soils Few filaments or I Thin, discontinuous pebble coatings faint coatings ΙI Continuous pebble Few to abundant nodules, flakes, coatings, some filaments interpebble fillings III Many nodules and Many interpebble fillings internodular fillings IV Laminar horizon Increasing carbonate impregnation overlying plugged horizon Secondary Material Example - Sand with trace to some silt Trace - 5-12% (by dry weight)

Little - 13-20% (by dry weight) - >20% (by dry weight)

Plasticity: Plasticity index is the range of water content, expressed as a percentage of the weight of the oven-dried soil, through which the soil is plastic. It is defined as the liquid limit minus the plastic limit. Descriptive ranges

used on the logs include:

Nonplastic (PI, 0-4)Slightly Plastic (PI, 4 - 15) Medium Plastic (PI, 15 - 30) Highly Plastic (PI,

Cobbles and Boulders

: A cobble is a rock fragment, usually rounded by weathering or abrasion, with an average diameter ranging between 3 and 12 inches (8 and 30 cm).

A boulder is a rock fragment, usually rounded by weathering or abrasion, with an average diameter of 12 inches (30 cm) or more.

- I. Remarks This column was provided on boring and trench logs for comments regarding drilling difficulty, number and size of cobbles or boulders encountered, loss of drilling fluid in the boring, trench wall stability, and other conditions encountered during drilling and excavations.
- J. Dry Density and Moisture Content The boring logs include a graphical display of laboratory test results for dry density (ASTM D 2937-71) in pounds per cubic foot and kilograms per cubic meter and moisture content (ASTM D 2216-71) in percent from representative samples taken during drilling. The symbols are explained at the bottom of the boring logs.
- K. Sieve Analysis The numbers represent the percentage by dry weight (ASTM D 422-63) of each of the following soil components:
 - GR Gravel, rock particles that will pass a 3-inch (76-mm) sieve and are retained on No. 4 (4.75 mm) sieve.
 - SA Sand, soil particles passing No. 4 sieve and retained on No. 200 (0.075 mm) sieve.
 - FI Fines, silt or clay soil particles passing No. 200 sieve.
- L. Atterberg Limits (LL and PI) -
 - LL Liquid Limit, the water content corresponding to the arbitrary limit between the liquid and plastic states of consistency of a soil (ASTM D 423-66).

- PL Plastic Limit, the water content corresponding to an arbitrary limit between the plastic and the semisolid state of consistency of a soil (ASTM D 424-59).
- PI Plasticity Index, numerical difference between the liquid limit (LL) and the plastic limit (PL) indicating the range of moisture content within which a soilwater mixture is plastic.
- NP Nonplastic.

M. Miscellaneous Information -

Elevations - indicated elevations on the logs are estimated from topographic maps of the study area, within an accuracy of half the contour interval.

Surficial

Geologic Unit - indicates the surficial geologic unit in which the activity is located.

Date Drilled - indicates the period from beginning to completion of the activity.

Drilling

Method - signifies the type of drilling procedure used such as rotary wash.

Hole Diameter - nominal size of boring drilled.

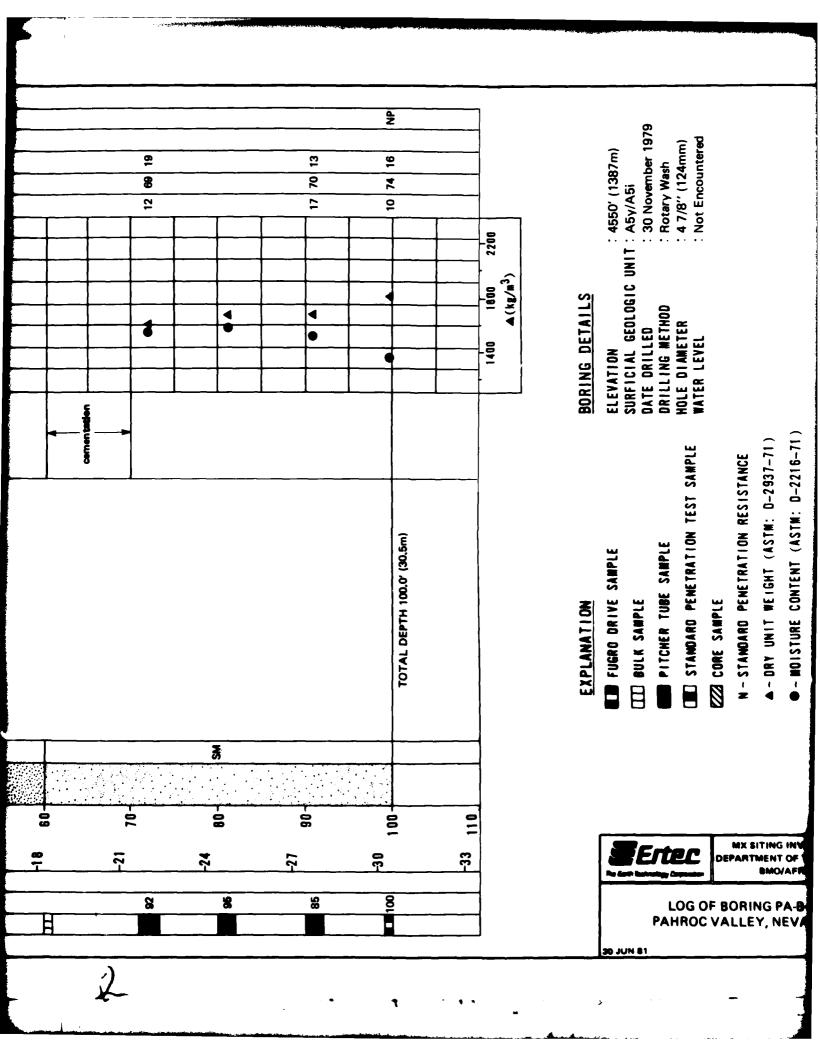
Water Level - indicates depth from ground surface to water table where encountered.

Trench Length - length at ground surface of final trench excavation.

Trench

Orientation - bearing of longitudinal trench centerline.

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SIEVE ANALYSIS	8	76			- 51		8				
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						<u> </u>	<u> </u>	<u> </u>	<u> </u>		<u> </u>
REMARKS							Γ				
SOIL DESCRIPTION	GRAVELLY SAND, brown to gray-brown, fine to coarse, poorly graded, medium dense to very dense, angular, calcareous;	to some fine to coarse gravel; trace blastic silt; sand (8.0' - 11.0').				SAND, gray-brown, fine to coarse, well graded, very dense, angular, calcareous; trace nonplastic silt; trace: fine gravel.	Interbedded layers of GRAVELLY SAND and SILTY SAND.	GRAVELLY SAND (SM, SP): brown to gray-brown, fine to coarse, poorly graded, very dense, angular, calcareous; little to	some nine to course gravel; little nonplastic slit. SILTY SAND (SM): gray-brown, fine to	, poorly graded, ionplastic siit; tr	
S	GRAV fine to	little				3 5 5	- •	O 54 > 4		0 =	
nzcz	GRAVI fine to	SP.	NS.		8	SW. SA SM gra	_ 4	X	2 # W		8
LITHOLOGY		ઝે			\$				X TO		8
LITHOLOGY		ઝે	WS -0-		20 						8
EET LITHOLOGY	0	ઝે				SW-SW-SW-SW-SW-SW-SW-SW-SW-SW-SW-SW-SW-S		8			, ,
METERS = = LITHOLOGY USCS	0	ઝે	-01		20	SW.		8			, ,
LITHOLOGY USCS	0	ઝે	-0-5-	001	20	SW-SSW-SSW-SSW-SSW-SSW-SSW-SSW-SSW-SSW-		\$8 175			, ,



A(kg/m³)

EXPLANATION

FUGRO DRIVE SAMPLE

DULK SAMPLE

PITCHER TUBE SAMPLE

(III) STANDARD PENETRATION TEST SAMPLE

BORING DETAILS

30 November 1979

: 4 7/8" (124mm) : Rotary Wash

DRILLING METHOD

HOLE DIAMETER NATER LEVEL

ELEVATION : 4550' (1387m) SURFICIAL GEOLOGIC UNIT: A5y/A5i DATE DRILLED

Not Encountered

ZZZ CORE SAMPLE

N - STANDARD PENETRATION RESISTANCE

■ - MOISTURE CONTENT (ASTM: D-2216-71)

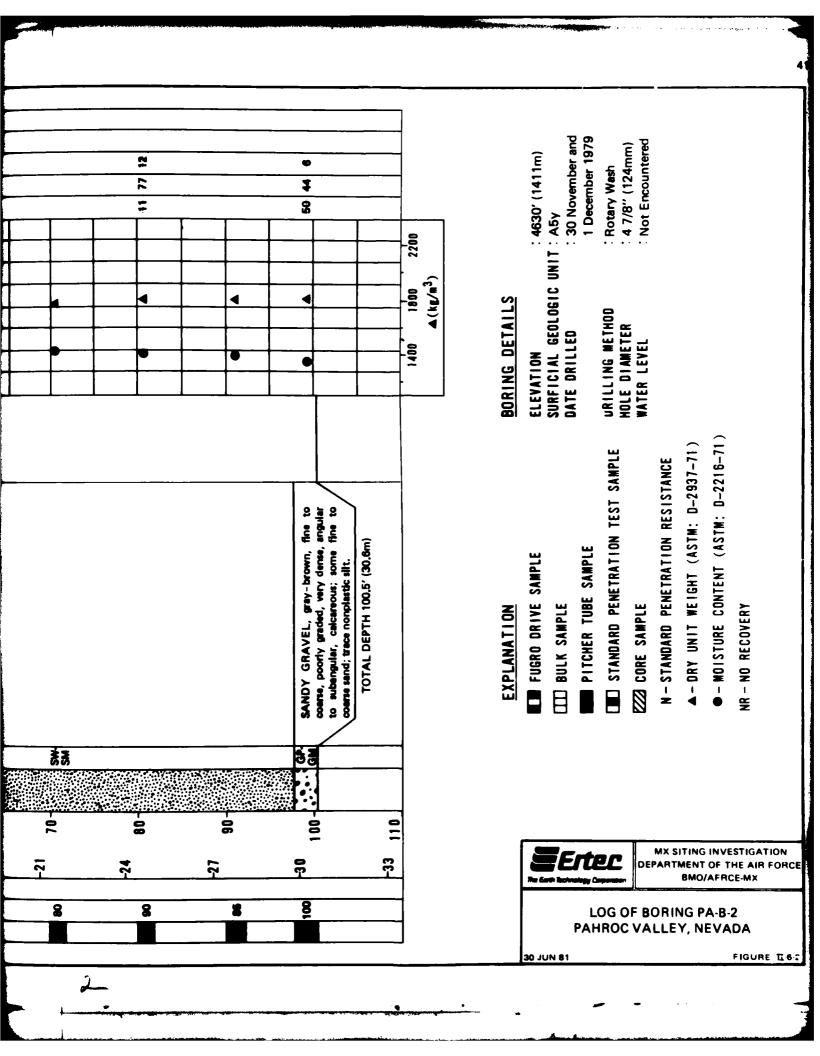
▲-DRY UNIT WEIGHT (ASTM: D-2937-71)

NR - NO RECOVERY

DEPARTMENT OF THE AIR FORCE BMO/AFRCE-MX

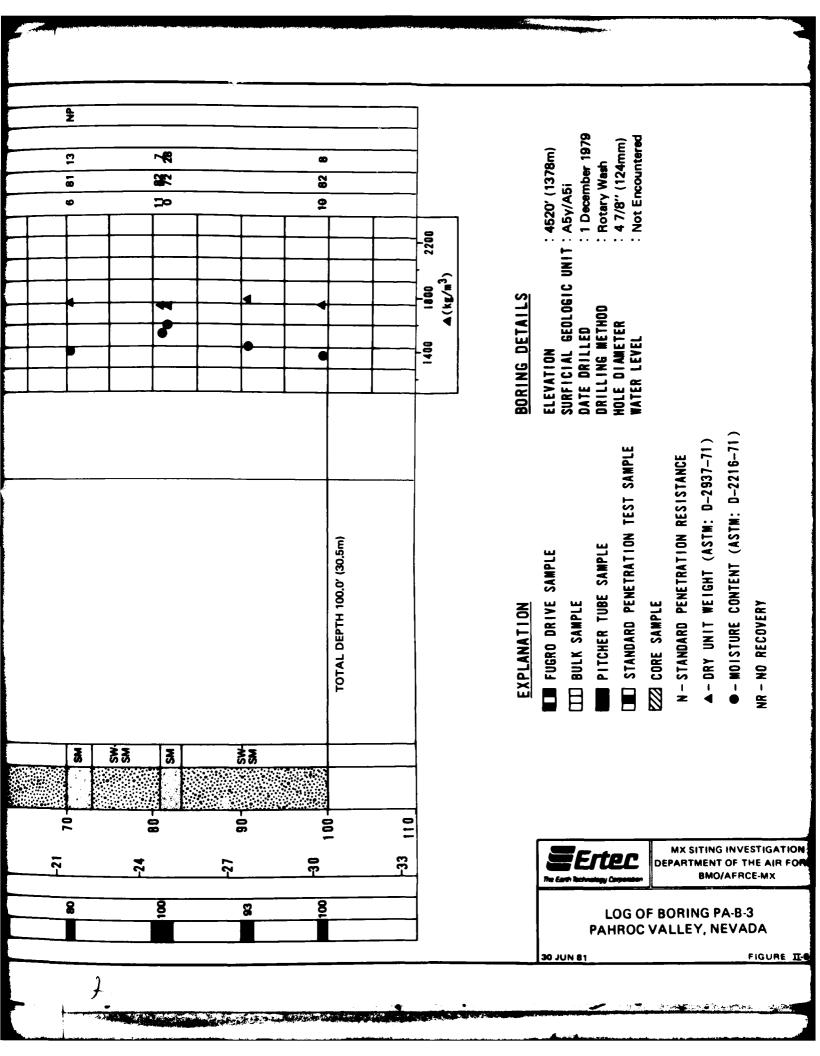
LOG OF BORING PA-B-1 PAHROC VALLEY, NEVADA

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8 +	5 10	•	• •			•		•					
REMARKS						T				<u> </u>		-	
SOIL DESCRIPTION		SILTY SAND, light brown to brown, fine to coarse, poorly graded, medium dense to dense anoular to subanquiar	calcareous; little nonplastic silt; none to trace fine gravel.			SAND, light brown, fine to coarse, well graded, dense, angular to subangular, cal-	careous; o ace norpassuc sin.			GRAVELLY SAND, gray-brown, fine to coarse, poorly graded, very dense, angular to subangular; some fine to coarse gravel.		SAND, brown to gray-brown, fine to coarse, very dense, angular to subangular, calcareous; trace fine gravel; trace nonplas-	de alt.
nzcz				ž,				N N		3			
THOLOGY	וו												
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SANPLE TYPE

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7.0 TRENCH AND TEST PIT LOGS

See Section 6.0, "Boring Logs," for explanation.

METERS 20	122	LITHOLOGY	RSCS	CONSISTENCY	SOIL DESCRIPTION	REMARKS	AN	I EV	LL	F
	0		SM	medium dense	SMLTY SAND, brown, fine to scarce, pearly graded, dry, subanquier, calcarceus; listle nemplastic silt; trace fine gravel; stage IV callabe (2.5' - 3.0').	vertical wells stable		ח		
-1	4			dense	TOTAL DEPTH 3.0' (0.8m)	opmontation at 3.0' exceeded expecity of Case 580C backhoo				
- 2	8-									
	8 -						1			
	10-									
-4	14-				·					
-5	10-									
	18-									
- 8	20-									

TRENCH DETAILS

SURFACE ELEVATION : 5080' (1640m) BATE EXCAVATED : 6 November 1979

SURFICIAL REGLOSIC UNIT: ASY TRENCH LENGTH : 6.0' (1.8m)

TRENCH ORIENTATION

: N-S



MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE BMO/AFRCE-MX

LOG OF TRENCH PA-T-1 PAHROC VALLEY, NEVADA

30 JUN 81

FIGURE IL7-1

viM-37

SSLTY SAND, brown, fine to ederen, poorly graded, slightly mobit, angular to submission dense dense submission dense dens	WLE SABPLE	PTN E	L!THOLOGY	USCS	CONSISTENCY	SOIL DESCRIPTION	REMA	RKS	AM	ALY	118		
medium pooling grades, slightly moles, aspectants to substance to substance and substa] = =						8.8	24	FI	LL	P
TOTAL DEPTH 6.0' (1.8m) TOTAL DEPTH 6.0' (1.8m) Securities Secu					medium	poorly graded, slightly moist, angular to subangular, calcareque; little nomplestic			2	82	16		
707AL DEPTH 6.0' (1.8m) TOTAL DEPTH 6.0' (1.8m) Sussession capacity of Case 580C backhoe excessed at 6.0' 124 14188	- 1	4-		SM	dense								
70TAL DEPTH 6.0' (1.8m) 10- 12- 18- 18-		6 -					,						
-3 10- 12- -4 14- 18-	- 2	•	[] }			TOTAL DEPTH 6.0' (1.8m)	Case	ity of 580C khoe					
124 -145 -8		8 -					at (B.0°					
-4 -9 18- -9 18-	-3	10-											
-5 18- -6	į	12-											
-5 18- -6	-4] :									
18-		14-		,									
	- 5	18-											
		18-											
	-•	20~											

SURFACE ELEVATION : 4620' (1378m)
BATE EXCAVATED : 6 November 1970

TRENCH LENGTH : 10.0" (A50

TRENCH ORIENTATION : E-W

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LOG OF TRENCH PA-T-2
PAHROC VALLEY, NEVADA

30 JUN 81

FIGURE 11-7-2

USAF-97

BULK SAMPLE	FEET #	LI THOLOGY	nscs	CONSI STENCY	SOIL DESCRIPTION	REMARKS	AN	A LY:		ī.	P
0	2		GP. GM	dense	SANDY GRAVEL, light brown, fine to coarse, poorly graded, dry, subangular to subrounded, calcareous; some fine to coarse sand; trace nonplastic silt.	vertical walls stable			12		
1	4-				TOTAL DEPTH 2.0' (0.6m)	excavation capacity of Case 580C backhoe exceeded at 2.0'					
- 2	8.					·					
-3	10-							:			
-4	12-										
	14-							! !			
-5	18-										
- 8	20-										

SURFACE ELEVATION

: 4715' (1437m)

DATE EXCAVATED

: 15 November 1979 .

SURFICIAL SECLOSIC UNIT: A5

TRENCH LENGTH : E-W

TRENCH ORIENTATION

: 8.0' (2.4m)



MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE BMO/AFRCE-MX

LOG OF TRENCH PA-T-3 PAHROC VALLEY, NEVADA

30 JUN 81

FIGURE IL7-3

VSAF-37

BULK SAMPLE	PTH H:	L! THOLOGY	nscs	CONSISTENCY	SOIL DESCRIPTION	REMA	RKS		A LYS			
E BOL	FEET	5		8				BR	SA	FI	LL	P
- 1	2 -		SW- SM	loose	GRAVELLY SAND, light brown, fine to coarse, well graded, dry, subangular, calcareous; little fine gravel; trace nonplastic silt; stage IV caliche (5.5' - 7.0').	vertici slow	al walts ghing	19	69	12		
- 2	6 .			very dense		vertica sta						
	8 -				TOTAL DEPTH 7.0' (2.1m)	cemen at 7,0' e capacity 580C be	xceeded of Case					
-3	10-							ļ				
	12-											
-4	14-						•					
- 5	16-											
	18-											
- 6	20-											

SURFACE ELEVATION

: 4550' (1387m)

DATE EXCAVATED

: 15 November 1979

SURFICIAL GEOLOGIC UNIT: A5y/A5i

TRENCH LENGTH TRENCH GRIENTATION : 11.0' (3.4m)

: E--W



MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE BMO/AFRCE-MX

LOG OF TRENCH PA-T-4 PAHROC VALLEY, NEVADA

30 JUN 81

-- AF-37

BULK SABPLE	NETERS A	PTH	LI THOLOGY	uscs	CONS! STENCY	SOIL DESCRIPTION	REMARKS		A LYS			
		FEET			3			GR	SA	FI	LL	P
	0	0		SW- SM	dense	SAND, red-brown, fine to coarse, well graded, slightly moist, subangular, calcareous; trace nonplastic silt; stage III - IV caliche (2.0' - 3.0').	vertical walls stable	,	88	11		
		•-			dense							l
	- 1	4	<u> </u>			TOTAL DEPTH 3.0' (0.9m)	cementation at 3.0' exceeded capacity of Case 580C beckhoe					
	- 2	8-										
		8-										
	- 3	10-										
	-4	12-										
		14-										
	-5	18-										
		18-							! 			
	†°	20-										

SURFACE ELEVATION : 4630' (1411m)

DATE EXCAVATED : 15 November 1979

SURFICIAL SEOLOGIC UNIT: A5y
TRENCH LENGTH : 8.0° (2.4m)
TRENCH ORIENTATION : E--W



MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE BMO/AFRCE-MX

LOG OF TRENCH PA-T-5 PAHROC VALLEY, NEVADA

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FIGURE II-7-6

VSAF-37

BULK SAMPLE	EPTH	LITHOLOGY	uscs	CONSISTENCY	SOIL DESCRIPTION	REMARKS	AN	IEV	118		
1766	2 -	.11	SP- SM	medium dense	GRAVELLY SAND, brown, fine to coarse, poorly graded, dry, subangular, calcareous; some fine to coarse gravel; trace nonplastic silt; occasional cobbles to 11" size.	vertical walls stable	T	SA		L	
- 2	8 -			very dense	TOTAL DEPTH 6,0' (1.8m)	excavation capacity of Case 580C backhoe exceeded at 6.0'					
- 3	10-		:								
- 5											
- 8	20-										

TRENCH DETAILS

SURFACE ELEVATION : 4990' (1521m) DATE EXCAVATED : 15 November 1979

SURFICIAL GEOLOGIC UNIT: A51/A5y TRENCH LENGTH : 10.0° (3.0m)

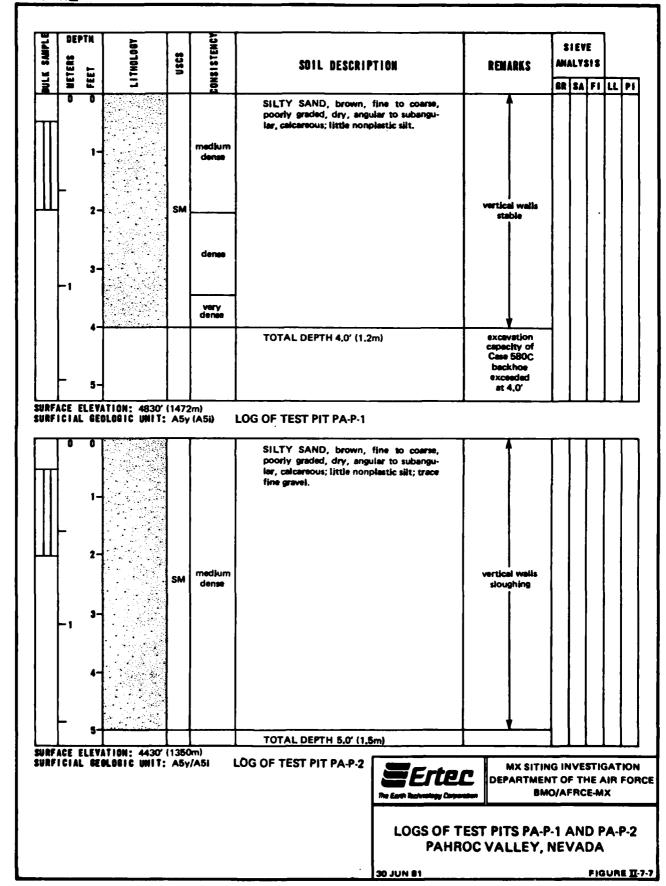
TRENCH ORIENTATION : E-W

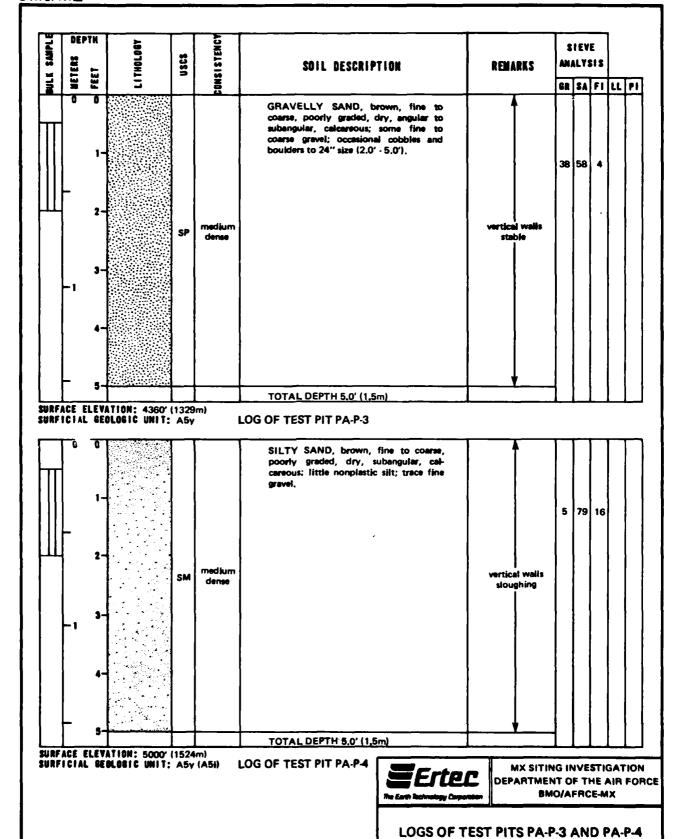
MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE BMO/AFRCE-MX

LOG OF TRENCH PA-T-6 PAHROC VALLEY, NEVADA

FIGURE II-7-6

USAF-37





PAHROC VALLEY, NEVADA

FIGURE 11-7-8

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NEK SAMPLE	NETERS A	PTH LIBI	LITHOLOGY	USCS	ONSISTENCY	SOIL DESCRIPTION	REM	ARKS	AM	1EVI	18		
	0	0 1- 2-		GP	medijum dense	SANDY GRAVEL, brown, fine to coarse, poorly graded, slightly moist, subangular, calcareous; some medium to coarse sand.		A walks	GR	SA	FI	u	PI
WRF	ACE ICIA	S- ELEV L GE	ATION: 4330' OLOBIC UNIT:	(1320 A5i	Om)	TOTAL DEPTH 5.0' (1.5m) LOG OF TEST PIT PA-P-5 SILTY SAND, red-brown, fine to coarse, poorly graded, slightly moist, angular to subangular, calcareous; some nonplastic silt; stage III - IV caliche (2.0' - 3.0').				73	22		_
		2-		SM	very dense	TOTAL DEPTH 3.0' (0,9m)	sta	al walls			23		
		4- 5-	<u> </u>	· .		, o many	at 3.0' e	ntation xceeded r of Case ackhos					
iurf iurf	ACE	F GE	ATION: 4520' GLOSIC UNIT:	1378 A5y	lm)	LOGS OF	DE		NT O	F TH	E-M	VIR I	FOI

BULK SANPLE	METERS 430		L 1 THOLOGY	uscs	CONSISTENCY	SOIL DESCRIPTION	REMARKS		A LY			
BULI		FEET	LIT		CON			GR	SA	FI	LL	Ī
	-	1 2		SM	dense	GRAVELLY SAND, brown, fine to coarse, poorly graded, slightly moist, angular to subangular, calcareous; little fine to coarse gravel; little nonplastic silt; stage III caliche (3.0' - 4.0').	vertical walls stable					
i	- 1	3-			very dense							
		4-										
					dense							
		5				TOTAL DEPTH 5.0' (1.5m)		1				l
	<u> </u> 	6-										
	- 2											
		7_										
	-	8 -										
		9 -			:							
	3	I O										
1												

SURFICIAL GEOLOGIC UNIT: A5y

LOG OF TEST PIT PA-P-7



MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE BMO/AFRCE-MX

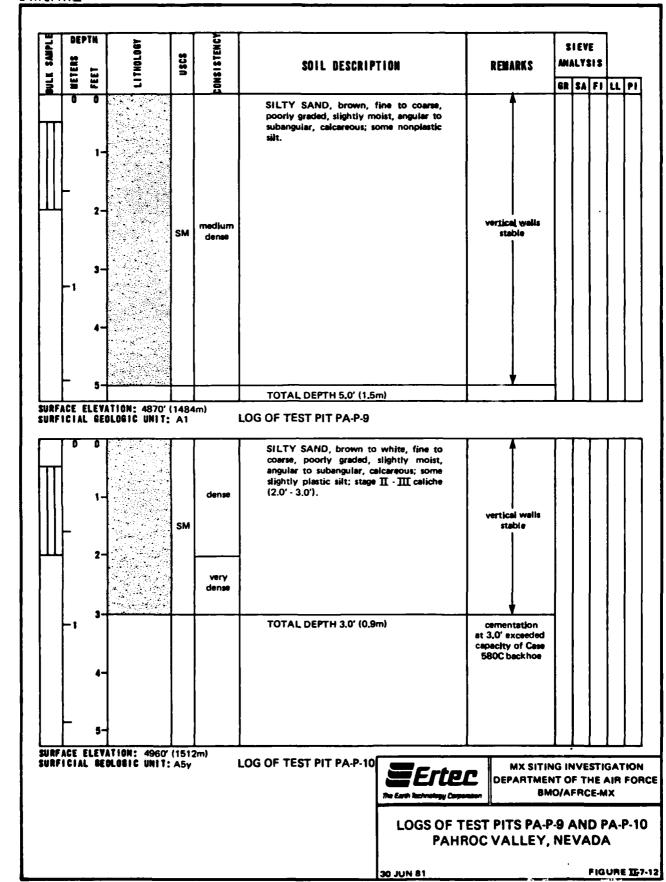
LOG OF TEST PIT PA-P-7 PAHROC VALLEY, NEVADA

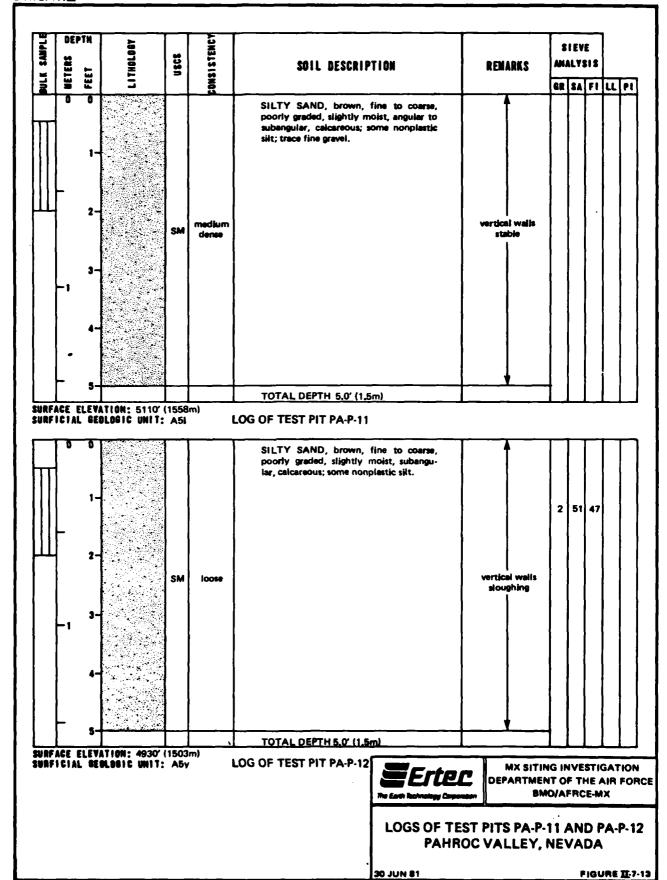
30 JUN 81

FIGURE II-7-10

FIGURE 11-7-11

BULK SAMPLE	EPTH E	LITHOLOGY	nscs uscs	COMS STENCY	SOIL DESCRIPTION		REMARKS		ALY	- VE 'S 18	ĺ	
	0	III		C 081	SAND, brown, fine to coarse, poorty graded, dry, subangular, calcareous; occasional cobbles to 11" size (0.0'-3.5'); thin lenses of gravel (0.0'-3.5').			er	84	FI	LL	Pi
	2 -		SP.	medium i dense		,	vertical walls sloughing					
	4 - 5 -				GRAVELLY SAND, brown, fine to coarse, poorly graded, dry to slightly moist, subangular, calcareous; little fine gravel; stage III caliche (5.5' - 7.0').							
- 2	6 - :			dense	TOTAL DEPTH 7.0' (2,1m)	,	rertical walls stable					
-	8 -					į						
- 3	10-							į				
BURFACI SURFIC		ATION: 4870' Ologic unit:	(148 A51/	4m) /A5y	LOG OF TEST PIT PA-P-8							
			- 4		EErte Manage Co		MX SITIF DEPARTMEN	IG II NT O NO/A	FT	HE	NIR	'IOI
					2		TEST PIT					





8.0 SURFICIAL SOIL SAMPLE LOGS

<u>Explanation</u>: Finalized logs of the surficial samples are presented in this section. Explanations of the column headings on the logs follow:

- A. Designations Surficial samples are identified as follows:
 - PA-CS-1
 - PA abbreviation for the valley (e.g., PA-Pahroc)
 - CS abbreviation for surficial sample
 - 1 number of activity
- B. Ground Surface Elevation Indicated elevations on the logs are estimated from topographic maps of the study area within an accuracy of half the contour interval.
- C. Surficial Geologic Unit Indicates the surficial geologic unit in which the activity is located.
- D. Depth Indicates depth interval for which soil description is given.
- E. USCS Unified Soil Classification Symbol; see Table II-6-1 of Section 6.0, "Borings Logs," for details of USCS.
- F. Soil Description Soil is described based on field visual descriptions and/or laboratory test results. See Section 6.0, "Boring Logs," for procedures of soil description.
- G. Sieve Analysis, LL and PI These are from results of laboratory tests. See Section 6.0, "Boring Logs," for explanation.

en ound Surface	SURFICIAL	DE PTH,		ORII REGARIETIAM	I -	IEV	_		
FEET (METERS)	UNIT	FEET (WETERS)	USES	2017 AESPELLIAN				111	P
4760 (1451)	ASI	0.0 - 2.0 (0.0 - 0.0)	SP-SM	GRAVELLY SAND, brown, fine to course, possity graded, angular to sub- angular, calcardous; some fine to course gravel; trase nonplastic sits.	36	57	7		
4620 (1408)	ASI	0.0 - 2.0 (0.0 - 0.0)	GP-GM	SANDY GRAVEL, brown, fine to searce, poorly graded, angular to sub- angular, calcareous; some fine to coarse send; trace nonpleatic sit.	66	22	10		
4320 (1317)	A1	0.0 - 1.5 (0.0 - 0.5)	SM	SILTY SAND, brown, fine to coarse, poorly graded, subenquier, calcareous; little nonpleatic allt; trees fine gravel.				!	
		1,5 - 2,0 (0,5 - 0,6)	GP	SANDY GRAVEL, brown, fine, peerly graded, subangular, calcareous; little fine to cease send.					
4300 (1330)	ABy/ABI	0.0 - 2.0 (0.5 - 0.6)	SM	SILTY SAND, brown, fine to medium, poorly graded, subanquier, calcareous; little nonplestic silt,					
4729 (1438)	ABy/ABI	0.0 - 2.0 (0.0 - 0. 0)	300	SILTY SAND, brewn, fine to coarse, poorly graded, subenquier, calcaroous; little nomplastic sits.					
4300 (1311)	ABUASy	0.0 - 2.0 (0.0 - 0.6)	300	SILTY SAND, brown, fine to coarse, poerly graded, angular to subangular, externous; little nonplexic silt.	3	*	13		
4600 (1300)	AS _W ASi	0.0 - 2,0 (0.0 - 0.0)	\$20	SILTY SAND, brown, fine to course, possity graded, angular to subangular, calcareous; little nonplastic silt; treesfine gravel; stage IV caliche (2.0°).					
4010 (1407)	ASy	0.0 - 2.0 (0.0 - 0. 8)	SM	SILTY SAND, brown, fine to course, poorly grades, angular to subangular, calcareous; some slightly plastic silt; trace fine gravel; stage II caliche (0.5' - 2.0').	;				
4890 (1496)	ASy	0.0 - 2.0 (0.0 - 0.6)	SM	SILTY SAND, brown, fine to coerse, poorly graded, angular to subangular, calearous; some slightly plastic sits.		:			
5020 (1530)	ASy	0.0 - 2.0 (0.0 - 0. 6)	SM	GRAVELLY SAND, brown, fine to coorse, poorly graded, angular to sub-angular, calcareous; some fine gravel; some nonpleatic silt; stage II - III callabe (1.5' - 2.0').	21	58	21		
	ELEWATION, FEET (NETERS) 4760 (1461) 4828 (1468) 4820 (1317) 4888 (1338) 4728 (1438) 4728 (1438) 4728 (1438) 4729 (1438) 4800 (1311) 4800 (1407)	### SUPPACE ELEVATION, FEET (METERS) ### 4780	ELEWATION, FEET (METERS) 4780	SUPFACE ELEWATION QUEDLOSIS FEET (INSTERS) UNIT (INSTERS) USCS FEET (INSTERS) UNIT (INSTERS) USCS FEET (INSTERS) UNIT (I	SERVATE FRET (NETERS) WIIT RESURCE FRET (NETERS) WIIT RESURE (NETERS) ASI C.O2.0 (Q.O0.0) ASI C.O2.0 C.O0.0) ASI C.O2.0 C	SSIL DESCRIPTION ARMARD CREATER CREATE	SBIFACE ELEVATION COLOR COLOR	SBILDESCRIPTION ERELENT UNIT (SETER) USCS SBILDESCRIPTION AMALYS IS ELEVATION CRETERS UNIT (SETERS) UNIT UNIT (SETERS) UNIT	SELEVATION SECRETIFY UNIT SELEVATION SELEVATI



LOGS OF SURFICIAL SOIL SAMPLES PAHROC VALLEY, NEVADA

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FIGURE II-1

9.0 EXPLANATION OF LABORATORY TEST RESULTS

Explanation: Laboratory test results are presented in this section. Table II-9-1 contains a summary of laboratory test results. This table shows results of sieve analysis; plasticity data; in-situ dry unit weight, moisture content, degree of saturation, and void ratio for drive and Pitcher samples; results of compaction tests; and specific gravity of solids. Other tests such as triaxial compression, unconfined compression, direct shear, consolidation, chemical, and California Bearing Ratio (CBR) are indicated on the table. Tables II-9-2 through II-9-4 and Figures II-9-1 through II-9-2 present results of direct shear, chemical, and CBR tests.

All tests were performed in general accordance with the American Society for Testing and Materials (ASTM) procedures. The following list presents the ASTM designations for the tests performed during the investigation.

Type of Test	ASTM	Designations
Particle Size Analysis	D	422-63
Liquid Limit	D	423-66
Plastic Limit	.D	424-59
Unit Weight	D	2937-71
Moisture Content	D	2216-71
Compaction	D	1557-70
Specific Gravity of Solids	D	854-58
Triaxial	D	2850-70
Unconfined Compression	D	2166-66
Direct Shear	D	3080-72
Consolidation	D	2435-70
Test for Alkalinity (pH)	D	1067-70
Water Soluble Sodium	D	1428-64
Water Soluble Chloride	D	512-67
Water Soluble Sulphate	D	516-68
Water Soluble Calcium	D	511-72
Calcium Carbonate	D	1126-67
California Bearing Ratio (CBR)	D	1883-73

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Explanation for the tables and figures presented in this section are as follows.

- A. Activity Number Boring, trench, test pit, or surface sample designation.
- B. Sample Number Prefix indicates the type of sample; explanation is at the bottom of the table.
- C. Sample Interval This is the depth range measured from ground surface over which the sample was obtained.
- D. Percent Finer by Weight Presents the results of laboratory particle size analysis (ASTM D 422-63) performed on representative soil samples at the depth indicated. The numbers represent the percent (by dry weight) of the total sample weight passing through each sieve size indicated.
- E. Atterberg Limits (ASTM D 423-66 and D 424-59)
 - LL Liquid Limit, the water content (as percent of soil dry weight) corresponding to the arbitrary limit between the liquid and plastic states of consistency of a soil (ASTM D 423-66).
 - PL Plastic Limit, the water content corresponding to an arbitrary limit between the plastic and the semisolid state of consistency of a soil (ASTM D 424-59).
 - PI Plasticity Index, numerical difference between the liquid limit (LL) and the plastic limit (PL) indicating the range of moisture content within which a soil-water mixture is plastic.
 - NP Nonplastic.

- F. USCS Unified Soil Classification Symbols are given here; see Table II-6-1 in Section 6.0, "Boring Logs," for complete details of USCS system.
- G. In Situ Presents results of tests on drive and Pitcher samples.
 - Dry Unit Weight Indicates dry unit weight of soil determined as per ASTM D 2937-71.
 - Moisture Content Weight of water reported in percent of dry weight of soil sample (ASTM D 2216-71).
 - Saturation The degree of saturation in a soil sample is defined as the ratio (in percent) of the volume of water to the volume of all voids in the soil.
 - Void Ratio The numerical ratio of the volume of voids to the volume of solids in a soil specimen.
- H. Compacted Indicates results of laboratory maximum dry density and optimum moisture content test as per ASTM D 1557-70.
- I. Specific Gravity of Solids (ASTM D 854-58) Indicates the ratio of 1) the weight in air of a given volume of soil solids at a stated temperature, to 2) the weight in air of an equal volume of distilled water at a stated temperature.
- J. Triaxial The triaxial compression tests were performed in accordance with the procedures of ASTM D 2850-70. The following explanations and definitions apply.

Triaxial Compression Test - A cylindrical specimen of soil is surrounded
by a fluid in a pressure chamber and subjected to an isotropic pressure. An additional compressive load is then applied,
directed along the axis of the specimen
called the axial load.

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Consolidated-Drained (CD) Test

- A triaxial compression test in which the soil was first consolidated under an all-around confining stress (test chamber pressure) and was then compressed (and hence sheared) by increasing the vertical stress. "Drained" indicates that excess pore water pressure generated by strains are permitted to dissipate by the free movement of pore water during consolidation and compression.

Consolidated-Undrained (CU)

Test

- A triaxial compression test in which essentially complete consolidation under the confining (chamber) pressure is followed by a shear test at constant water content.

Confining Pressure

(a3)

 The isotropic chamber pressure applied to the soil specimen during consolidation and compression.

Maximum Deviator

Stress

(01-03)

- The difference between the major and minor principal stresses in the specimen at failure. The major principal stress on the specimen is equal to the unit axial load plus the chamber pressure and the minor principal stress on the specimen is equal to the chamber pressure.
- Strain Rate Axial strain, ϵ , at a given stress level is defined as the ratio of the change in length (ΔL) of the specimen to the original length of the specimen (L_O). The rate of strain was controlled during the test so that this ratio increased at equal increments for each

minute of testing.

- Back Pressure Pressure in excess of atmospheric applied to the pore water of a soil sample. Back pressure is usually applied to (1) increase saturation of the sample, or (2) simulate the actual in-situ pressure regime.
- K. Unconfined Compression Test procedures were as described in ASTM D 2166-66. Unconfined compressive strength is

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defined as the load per unit area at which an unconfined prismatic or cylindrical specimen of soil will fail in a simple compression test. In these methods, unconfined compressive strength is taken as the maximum load attained per unit area or the load per unit area at 20 percent axial strain, whichever occurred first during the performance of a test.

- L. Direct Shear The procedures of ASTM D 3080-72 were followed for direct shear testing. In this test, soil under an applied normal load is stressed to failure by moving one section of the soil container (shear box) relative to the other section. Normal stress is the value of load per unit area acting perpendicular to the plane of shearing. Maximum shear strength is defined as the maximum resistance (ksf) of a soil to shearing (tangential) stresses.
- M. Consolidation (ASTM D 2435-70) A consolidation test is a test in which a cylindrical soil specimen is laterally confined in a ring and compressed between porous plates. The term "consolidation," as used here, indicates the gradual reduction in volume of the soil mass resulting from an increase in compressive stress (axial load per unit area).
- N. Chemical The chemical tests performed on soil samples included: pH; water soluble sodium, chloride, sulphate, calcium; and calcium carbonate content. pH is an index of

the acidity or alkalinity of a soil in terms of the logarithm of the reciprocal of the hydrogen ion concentration.

ASTM test procedure designations for these chemical tests are included in the list on the first page of these Explanations.

O. CBR - California Bearing Ratio (CBR) is the ratio (in percent) of the resistance to penetration developed by a subgrade soil to that developed by a standard crushed-rock base material. The procedures for conducting a CBR test were as outlined in ASTM D 1883-73. The materials tested for CBR were also analyzed for particle-size distribution (ASTM D 422-63) and compaction characteristics (ASTM D 1557-70). The term "percentage of maximum density" indicates the ratio (as a percentage) of the compacted sample dry unit weight to maximum dry density obtained in the laboratory from ASTM D 1557-70, "Moisture-Density Relations of Soils Using 10-pound (4.5-kg) Hammer and 18-inch (457-mm) Drop."

D-10	40.2 - 40.9	12.25 - 12.47	11_	\perp		
P-13	71.8 - 72.6	21.88 - 22.13		100	93	93
P-14	81.1 - 81.9	24.72 - 24.96				
P-15	90.6 - 91.6	27.61 - 27.92	1 1	100	95	95
D-16	99.3 - 99.8	30.27 - 30.42			100	97
P-1	0.8 - 1.9	0.24 - 0.58				
P-2	3.8 - 4.3	1.16 - 1.31				
P-3	6.8 - 7.6	2.07 - 2.32	T - 1 -			
P-4	8.8 - 9.6	2.68 - 2.93				
P-5	11.3 - 12.1	3.44 - 3.69				
D-6	15.2 - 15.7	4.63 - 4.79	·		100	99
P-7	20.8 - 21.6	6.34 - 6.58	1			100
P-8	25.8 - 26.6	7.86 - 8.11				
P-9	30.8 - 31.6	9.39 - 9.63	1			
P-10	40.8 - 41.7	12.44 - 12.71		100	93	83
P-11	50.8 - 51.6	15.48 - 15.73			100	99
P-12	60.0 - 60.9	18.29 - 18.56				
P-13	70.8 - 71.6	21.58 - 21.82				
P-14	80.8 - 81.8	24.63 - 24.93			100	97
P-15	90.8 - 91.7	27.68 - 27.95				
P-16	98.9 - 99.6	30.14 - 30.36		100	92	63
P-1	0.8 - 1.6	0.24 - 0.49			100	98
P-2	3.8 - 4.6	1.16 - 1.40]			
P-3	6.8 - 7.6	2.07 - 2.32			100	97
P-4	10.8 - 11.6	3.29 - 3.54				
P-5	15.8 - 16.6	4.82 - 5.06				100
P-6	20.8 - 21.6	6.34 - 6.58				
P-7	25.8 - 26.6	7.86 - 8.11		100	82	78

1		SM	106.4	1705	7.6	35.0	0.58			
	7 1	SM	99,9	1600	13.5	53,3	0.69			
		SM	104.6	1676	14.4	63.9	0.61			
		SM	105.0	1682	12.6	56.2	0.61			<u> </u>
		NP SM	113,8	1823	7.5	42.3	0.48			
		SM	102.1	1636	5.3	22.1	0.65			
		SM	117.5	1882	6.5	40.3	0.43		<u> </u>	<u> </u>
		SM	105.8	1695	6.6	30.0	0.59			
		NP SM	106.5	1706	6.3	29.0	0.58			<u> </u>
		SM	104.9	1680	9.9	44.0	0.60		<u> </u>	
		SM	111.3	1783	7.9	41.3	0.51			<u> </u>
 		NP SW-SM	108.0	1730	8.5	40.9	0.56			
		SW-SM	106.8	1711	9.9	46.3	0.58	I		<u> </u>
		SW-SM	107.5	1722	7.8	37.0	0.57			
	1 1 1	SP	109,8	1759	12.4	62.8	0.54			<u> </u>
	1	SW-SM	104.3	1671	14.7	64.4	0.62			
	1 1	SW-SM	113.0	1810	9.7	53.6	0.49			
		SW-SM	111.9	1793	9.3	49.5	0.51			
		SW-SM	112,6	1804	9.1	49.8	0.50			
$\neg +$		SW-SM	113,7	1821	8.7	48.9	0.48			
	1 1 -1	GP-GM	112.6	1804	7.2	39.4	0.50			
$\neg \uparrow \neg$		1								
	1 1 1	SM	95.5	1530	5.5	19.4	0.76			
		SM	106.1	1700	7.5	34.5	0.59			
$\neg \vdash$		SM	107.1	1716	6.3	29.6	0.57			

<u> </u>											
<u> </u>		C	OMPACTE)		(g)	<u>~ 5</u>		3		
		MAXI	MUM	2 SE	2 ~ 2	AL (SS		M	AL	(I
SATTEMENT (X)	اء_ا	DRY DE		OPTIMUM Moisture (\$)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL (d)	unconfined Compression	DIRECT SHEAR	CONSOLIDATION	CHENICAL	
	VOID RATIO	(pcf)	(kg/m ³)		SPE SRA	TRI		33		CHE	CBR
17.6	0.74	(per)	(
13.6	0.58									*	
65.3	0.78						 			*	
68.3	0.66							*		*	
46.6	0.54										
32,1	0.63										\vdash
71.5	0.70										
20.7	0.52							*			
43.0	0.60						1				
35.0	0.58										\vdash
53 ,3	0.69						-				
63.9	0.61										
56.2	0.61				_						
42.3	0.48										
22.1	0.65										
40.3	0.43										
30.0	0.59										
29.0	0.58										
44.0	0,60										
41.3	0.51							*			
40.9	0.56										
46.3	0.58										
37.0	0.57										
62.8	0.54										
64.4	0.62		L							*	L
53.6	0.49			 							
49.5	0.51						 				
49.8	0.50										
48.9	0.48		L	ļ			ļ			<u> </u>	
39.4	0.50		 	L			-				\vdash
10.4	0.70						├				—
19.4 34.5	0.76		 -	 			├			 	
29.6	0.59		 	 		 	┼─┤	┝┯┤		 	$\vdash \!$
	0.57			 		<u> </u>	├				$\vdash \dashv$
40.2	0.55		 			<u> </u>	├				├─┤
48.7 46.3	0.66			 		<u> </u>	┼─┤			\vdash	$\vdash \vdash \vdash$
47.9	0.73 0.58			 			\vdash			-	\vdash
61.2				 			 			 -	$\vdash \vdash \vdash$
38.9	0.71			 			╁─┤	\vdash		 	┝─┤
36.9 37.6	0.49			 							├─┤
34.8	0,55		 	 -		<u> </u>	 			 	┝─┤
~.0	U.08			بسيا							



SUMMARY OF LABORATORY TEST RESULTS PAHROC VALLEY, NEVADA PAGE 1 OF 2

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TABLE II-9-1

7

70.0 - 70.8	21.34 - 21.58	1 1	1_		1	100	99
80.8 - 81.6	24.63 - 24.87					100	99
81.6 - 82.5	24.87 - 25.15						
90.8 - 91.4	27.68 - 27.86						
99.0 - 99.8	30.18 - 30.42						100
					1		
0.5 - 2.0	0.15 - 0.61						100
							
0.5 - 2.0	0.15 - 0.61	igspace				100	99_
							
<u> 0.5 - 2.0</u>	0.15 - 0.61	↓ ——		—	100	85	69
		 -		_	+	100	
0.5 - 2.0	0.15 - 0.61	+			1	100	93
05.00	0.15 0.61	╂┈╌┼╴			+		100
0.5 - 2.0	0.15 - 0.61	╀		-	+		100
0.5 - 2.0	0.15 - 0.61	╁┈╁			100	90	79
0.3 - 2.0	0.15-0.01	╂─┼		+	100	30	/9
0.5 - 2.0	0.15 - 0.61	 			100	88	75
<u> </u>	0.10 0.01	+-+			+	55	<u> </u>
0.5 - 2.0	0.15 - 0.61	╅			†	100	99
		1 1		_	T		
0.5 - 2.0	0.15 - 0.61	t			 	100	97
		 		1	 	100	
0.5 - 2.0	0.15 - 0.61				1	100	99
				1			
0.5 - 2.0	0.15 - 0.61				100	93	77
0.5 - 2.0	0.15 - 0.61				100	69	47
0.5 - 2.0	0.15 - 0.61					100	99
0.5 - 2.0	0.15 - 0.61		1	ı	100	97	88

- [79	38	19	13	т—	7	1	Τ-	NP	-	-	T				_	_				
	68	25	11	7	 	+	╂—	+-	INP	SM	109.7	1757	9.1	46.1	0.54		L	L	L		<u></u>
-	93		38	28	 	 	 	┼	┼	SW-SM	108.3	1735	13.2	64.4	0.56		L				<u> </u>
		 	 ==	╁┈	 	+	╂─╴	+-	├	SM	108.4	1737	14.9	72.9			<u></u>	<u> </u>	Ĺ <u> </u>		<u> </u>
	70	25	12	8	 	╅—	+	+	 -	SW-SM	110.7	1773	9,9	51.4	0.52						
		 			1	+	+	+-	 -	SW-SM	109.3	1751	7.7	38.5	0.54					ـــــــا	↓
	79	43	23	18	† —	 	 	+	╂	SM		 	 	 	ļ			L		 _	↓
		Ţ —				 	†	 	 	SIVI	 -	 	 	<u> </u>	ļ	123.2	1974	10.0	2.66	 	↓
	89	47	21	16	1	1	†	╆┈	┢╌┤	SM			├ ──			1011	1	L	 -	 	├ —
		Γ				 	1	 	+				├ ──	 		121.0	1938	11.2	<u> </u>		
	43	27	16	12		1	 	 	\vdash	GP-GM			├ ──-	├—		<u> </u>	 _	 	<u> </u>		├ ─
Н										9. 9.11			 	 	 		├	 -	}	} -	├
Н	70	45	18	12						SW-SM				 			 	 	 	 	
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Н	90	44	16	11	ļ					SW-SM			 	 			 	 	 	 	
Н	58				<u> </u>	↓							 				 	 	 	 	
Н	28	32	14	9	ļ		<u> </u>			SP-SM			t			118.0	1890	12.0	2.67	†	
H	45	17	6		<u> </u>	₩	!	lacksquare					<u> </u>			11313	1.555	1 213		1	<u> </u>
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H		<u> </u>		23		{	 	$\vdash \dashv$		SM											
П	92	81	64	47				$\vdash \dashv$											<u> </u>		$oldsymbol{ol}}}}}}}}}}}}}}}}}}$
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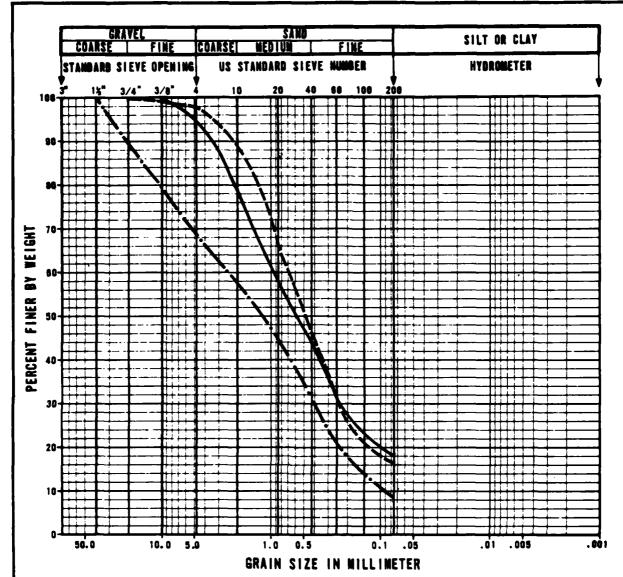
t	OMPACTE	0		a	0 =		8		
DI	MUM Py 12N	PT INUM O I STURE (\$)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL (d)	UNCONFINED COMPRESSION	DIRECT SHEAR	CONSOLIDATION	CHEMICAL	CBR
2	(kg/m³)	0.	2 3 2	1	5 5	0 0	8		5
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2	1974	10.0	2.66						*
9	1938	11.2	L			L			*
-	 	} <u>'</u>							
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	†								
1.0	1890	12.0	2.67			├			*
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SUMMARY OF LABORATORY TEST RESULTS PAHROC VALLEY, NEVADA PÅGE 2 OF 2

30 JUN 81

TABLE II-9-1



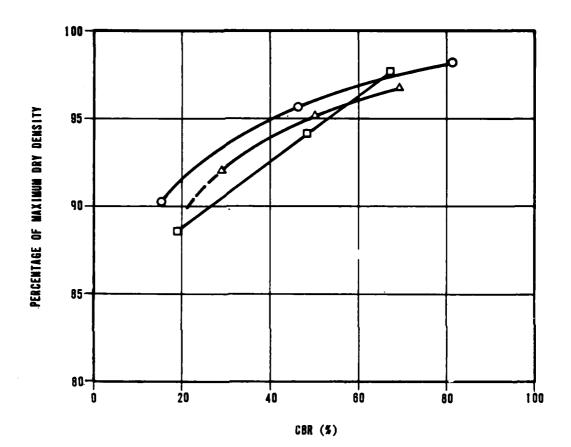
SYMBOL	COMPOSITE SAMPLE	ACTIVITY	SAMPLE	SOIL			
	NUMBER	NUMBER	FEET	METERS	TYPE		
-	Α	PA-T-1	0.5 - 2.0	0.15 - 0.61	SM		
	В	PA-T-2 -	0.5 - 2.0	0.15 - 0.61	SM		
	C	PA-T-6	0.5 - 2.0	0,15 - 0,61	SP-SM		
			_ :				



GRAIN SIZE CURVES, CBR TESTS PAHROC VALLEY, NEVADA

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FIGURE TH-1



SYMBOL	COMPOSITE SAMPLE NUMBER	SOIL Type
0	Α	SM
	8	SM
Δ	С	SP-SM



CALIFORNIA BEARING RATIO (CBR) CURVES PAHROC VALLEY, NEVADA

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FIGURE 11-0-2

BORING	SAMPLE	SAMPLE I	NTERVAL	SOIL	NORMAL	STRESS	MAXIMUM SHEAR STRENGTH				
NG.	NO.	FEET	METERS	TYPE	ksf	kM/m²	ksf	kN/m-2			
PA-B-1	P-4	9.3 - 10.0	2.83 - 3.05	SP-SM	1.0	48	1,27	61			
					1.5	72	1.84	88			
					2.0	96	2.22	106			
PA-B-1	D-8	25,2 - 25,9	7,68 - 7.89	SW-SM	2.5	120	3.40	163			
					3.8	182	4.08	224			
					5.0	239	6.35	304			
							<u></u>				
PA-B-2	D-6	15.2 - 15.7	4.63 - 4.79	SM	1.5	72	2.36	113			
					2.3	110	3.83	183			
					3.0	144	4.43	212			
PA-B-3	P-3	6.8 - 7.6	2.07 - 2.32	SM	0.5	24	0.91	144			
					0,8	38	1.12	54			
					1.0	48	1.51	72			
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DIRECT SHEAR TEST RESULTS PAHROC VALLEY, NEVADA

30 JUN 81

TABLE 120-2

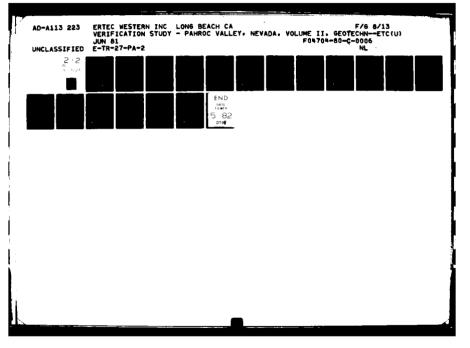
3	NATE	mg/kg	3	2		6	2	ტ	-	yg.	n							
CALC	CALC 1 UM CARBONATE		113	212	71	243	137	143	131	235	183							
	CALCIUM	ng/kg	52	22	27	æ	ಜ	37	æ	19	23							
MBLE	\vdash					_			_									
WATER SOLUBLE	SULPHATE	mg/kg	~	1	131	~	~	23	5	84	20							
3	CHLORIDE	mg/kg	9 >	112	170	11	11	37	16	61	35							
	SODIUM	ng/kg	13	238	370	2	43	8	81	"	9							
<u> </u>		•			<u> </u>													
	ā		8.4	9.2	8.6	8.5	8.5	8.3	8.5	8.5	7.3			_				L
	SOL		WS-dS	SP-SM	SP-SM	SW-SM	SP-SM	NS.	SW-SM	₹	SM							
		:RS	0.58	1.83 - 1.95	3.05	15.48 - 15.73	8.11	21.58	27.86	0.61	0.61				•			
	SAMPLE INIEKTAL	METERS	0.27 - 0.58	1.83	2.83 - 3.05	15.48	7.86 - 8.11	21.34 - 21.58	27.68 - 27.86	0.15 - 0.61	0.15 - 0.61							
			6	-	o	9.	3.6	9.8	•	٥	0							
	SA	FEET	0.9 - 1.9	6.0 - 6.4	9.3 - 10.0	50.8 - 51.6	25.8 - 26.6	70.0 - 70.8	90.8 - 91.4	0.5 - 2.0	0.5 - 2.0							
	SAMPLE No.		P.1	P.3	7	P-11	P.7	P-12	P-14	占	<u>1-</u> 4							
	ACTIVITY S		PA-8-1			PA-8-2	PA-8-3			PA-P-12	PA-CS-27							

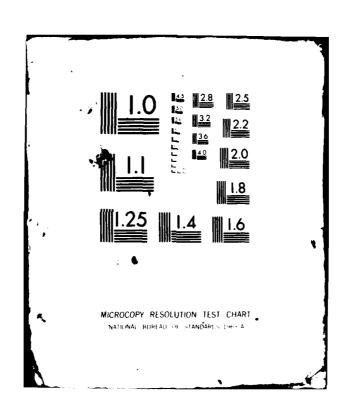


SUMMARY OF CHEMICAL TEST RESULTS PAHROC VALLEY, NEVADA

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TABLE IL-3





C 88	(\$)	18	9†	15			29	61	19			69	9	58						
PERCENT OF MAXIMUM	DRY DENSITY	286.2	296.7	90.2			97.6	1.14	88.6			96.7	1.98	92.0			·			
COMPACTED MOISTURE	(\$)	10.4	10.5	10.5			11.6	11.4	11.6			11.8	11.7	11.9						
CTED	kg/83	1838	1889	1780			1892	1823	1719			1828	1799	1740						
COMPACTED DRY DENSITY	pcf		117.0	111.1			118.1	113.8	107.3			114.1	112.3	108.6						
OPT IMUM Moisture	(\$)						11.2					12.0							•	•
MAXIMUM DRY DENSITY	kg/m3	1974				1938					189.0									
MAX DRY O	pc f			123.2					121.0			118.0								
SPECIFIC	GKAVIIT	2.66												2.67						
ATTERBERG LIMITS	ī																			
ATTE	11																			
PERCENT	#200	85				16					•									
		SM				SM							SP-SM							
COMPOSITE	NUMBER	<				6						,	ပ							



CALIFORNIA BEARING RATIO (CBR) TEST RESULTS
PAHROC VALLEY, NEVADA

30 JUN 81

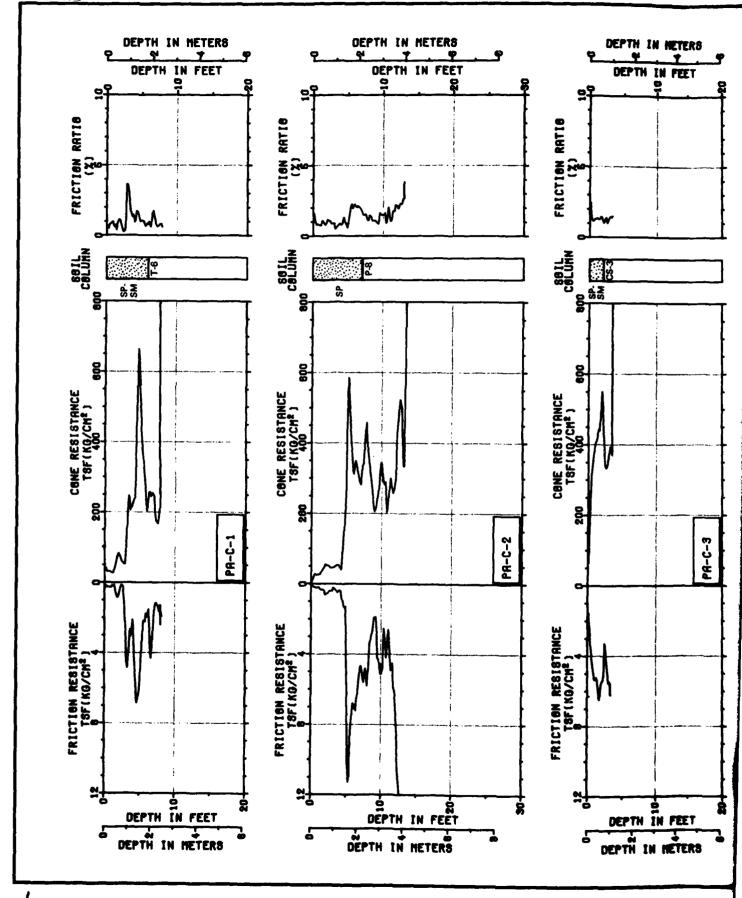
TABLE 1144

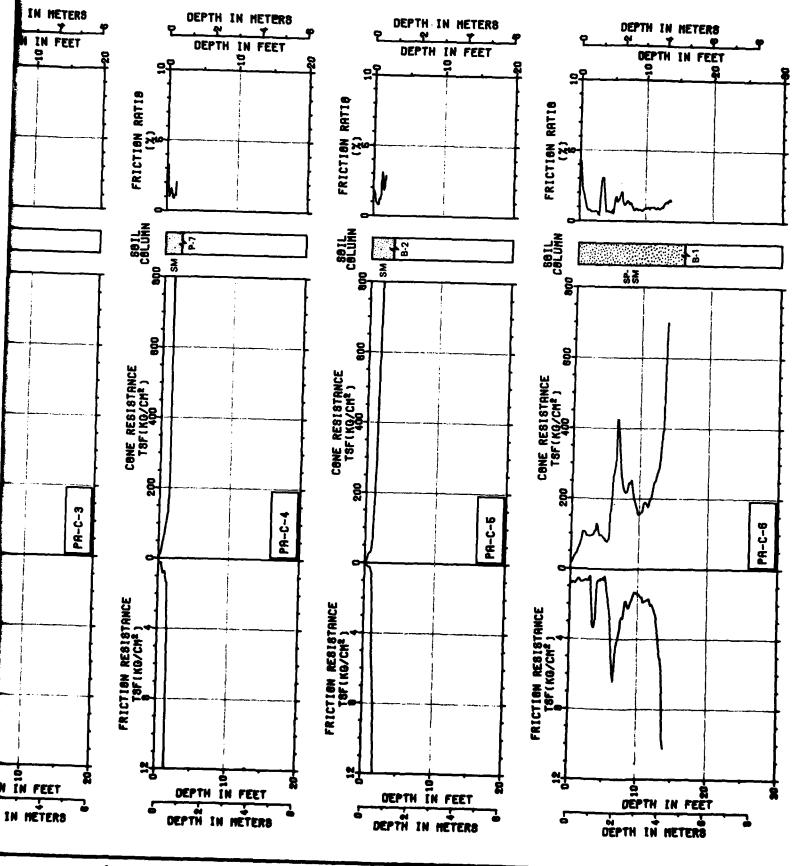
10.0 CONE PENETROMETER TEST RESULTS

Explanation: The results of all cone penetrometer tests are
presented in this section. Explanations of the test results are
as follows:

- A. Depth Corresponds to depth below ground surface.
- B. Friction Resistance The resistance to penetration developed by the friction sleeve, equal to the vertical force applied to the sleeve divided by its surface area. This resistance is the sum of friction and adhesion.
- C. Cone Resistance The resistance to penetration developed by the cone, equal to the vertical force applied to the cone divided by its hosizontally projected area.
- D. Friction Ratio The ratio of friction resistance to cone resistance.
- E. Designation Each cone penetrometer test is identified by a number: for example C-1.
 - C abbreviation for the CPT
 - 1 number of the test
- F. Soil Column A graphical presentation of the soil type versus depth at each cone penetrometer test location. The Unified Soil Classification Symbol (see Table II-6-1) for each different soil type is listed immediately to the left of the soil column. Immediately below the soil column, the activity number for the corresponding boring, trench, test

pit, or surficial soil sample at each CPT location is given.





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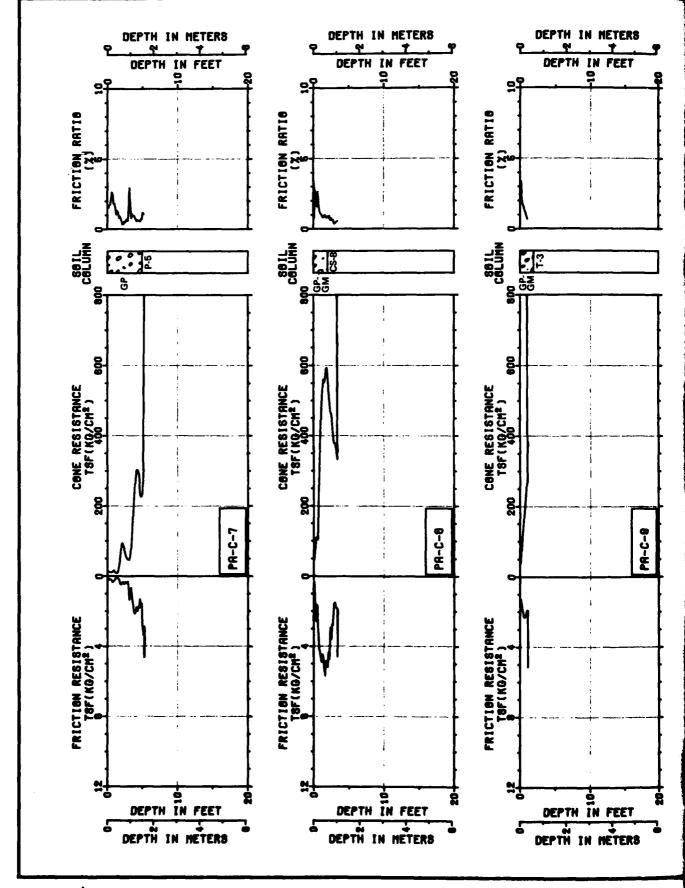




CONE PENETROMETER TEST RESULTS PAHROC VALLEY, NEVADA PAGE 1 OF 5

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FIGURE 11-10-1

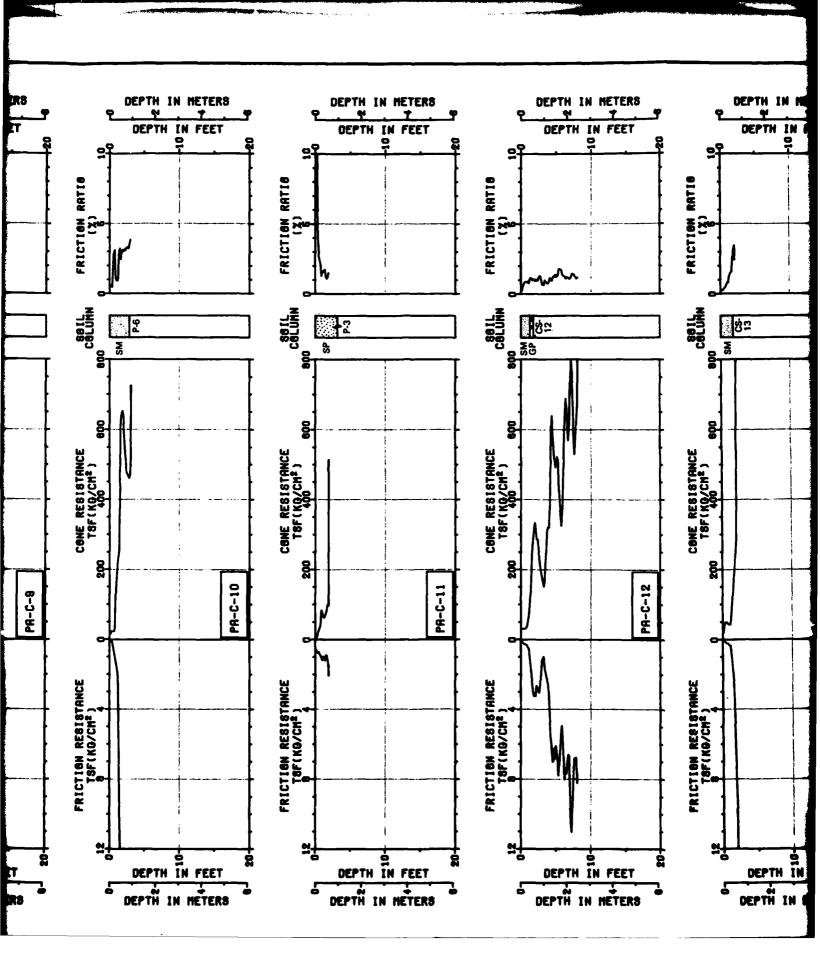


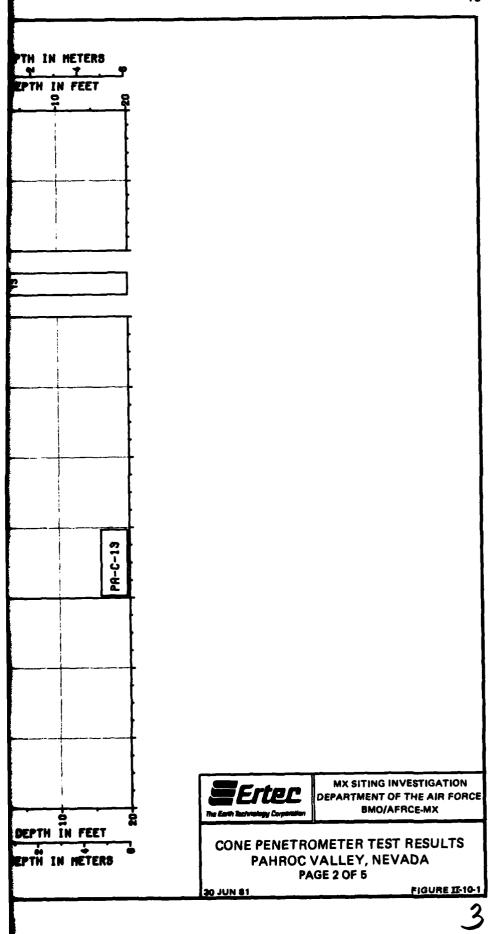
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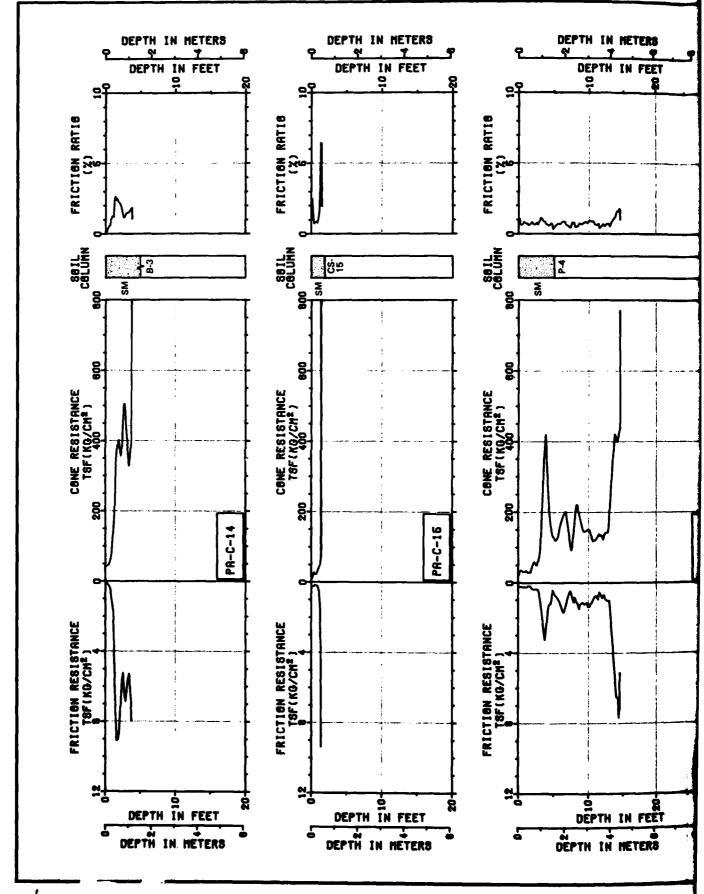
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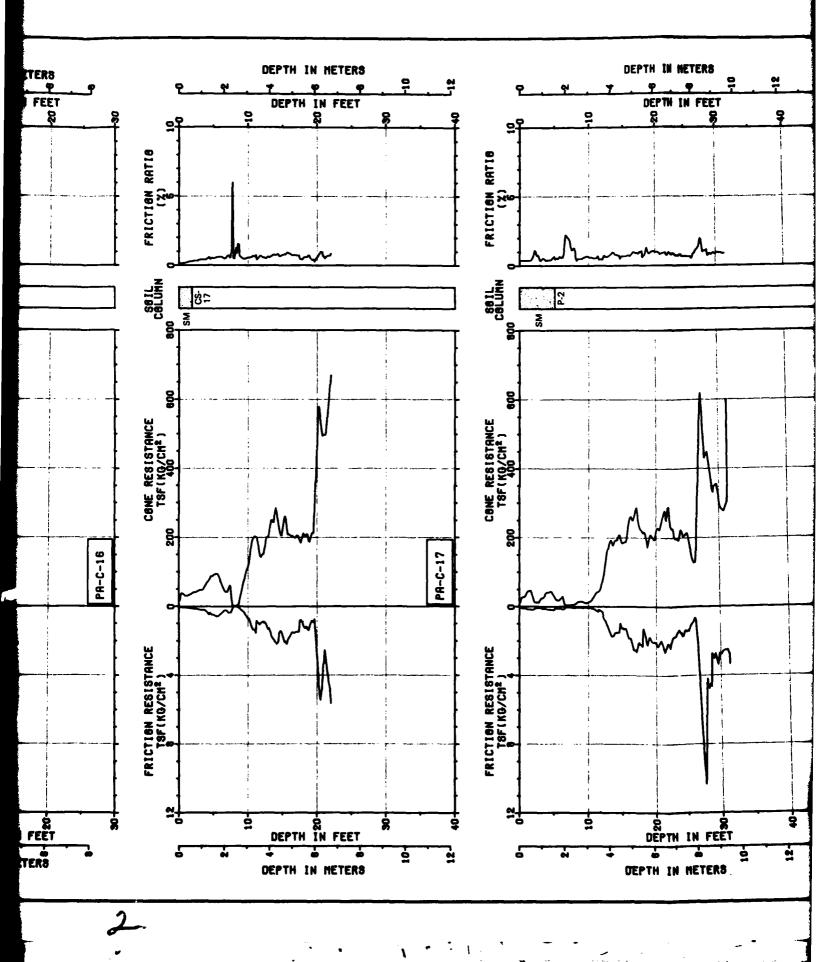
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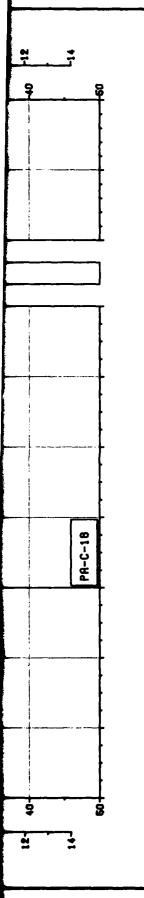
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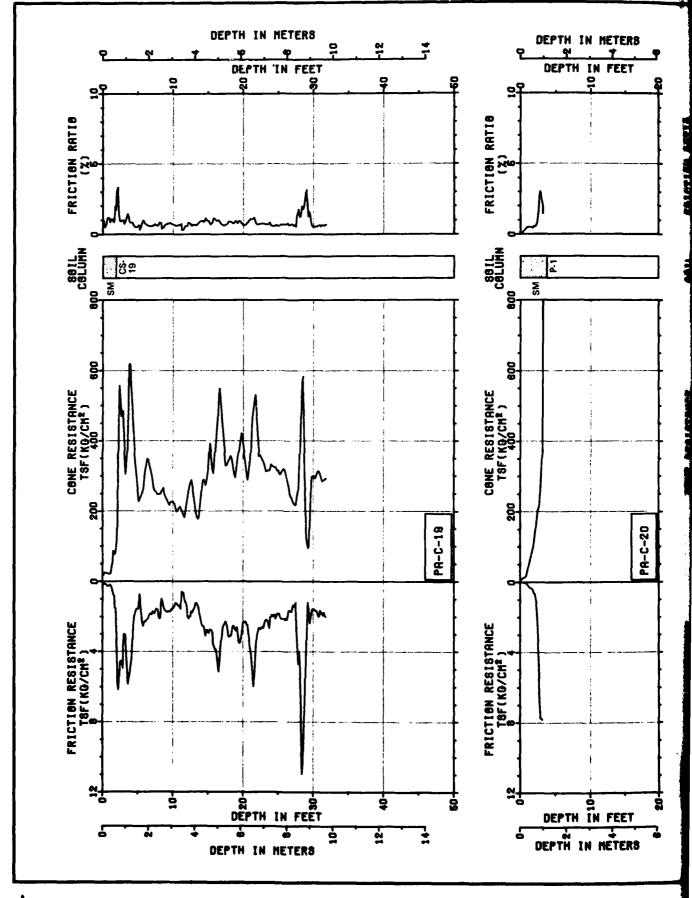


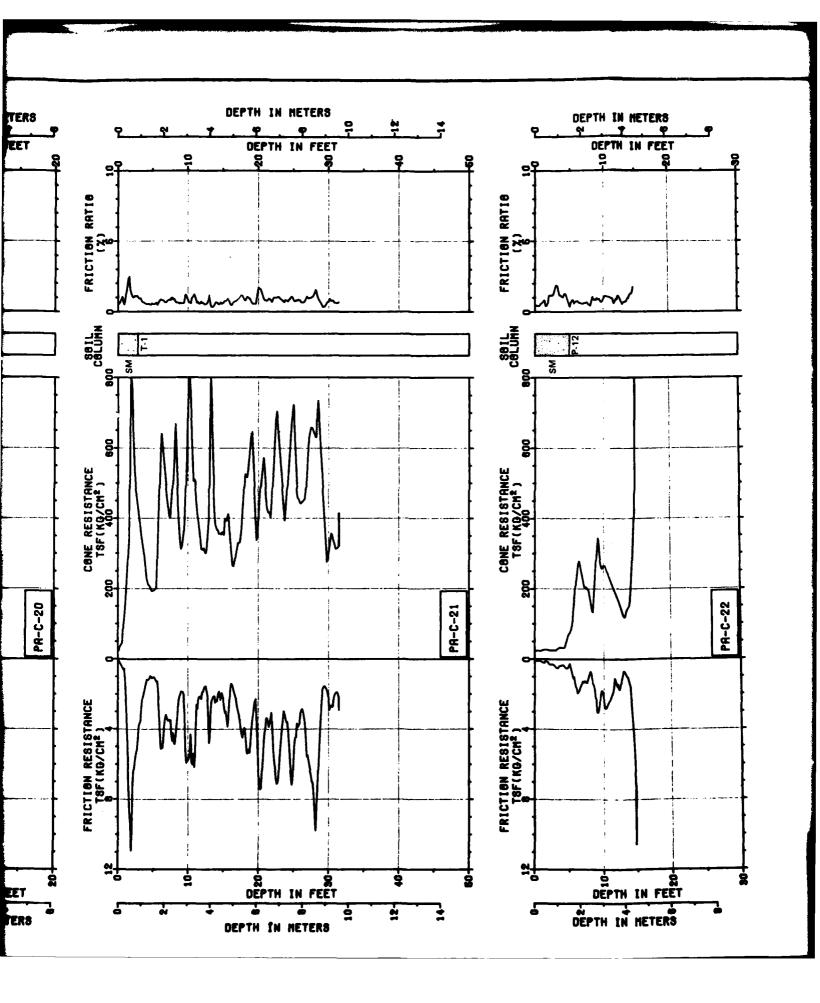


CONE PENETROMETER TEST RESULTS PAHROC VALLEY, NEVADA PAGE 3 OF 5

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FIGURE II-10-1









CONE PENETROMETER TEST RESULTS
PAHROC VALLEY, NEVADA
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FIGURE II-10-1

2

DEPTH IN FEET

DEPTH IN METERS

DEPTH IN FEET

DEPTH IN HETERS

